

129F

IMPROOF: INTEGRATED MODEL GUIDED PROCESS OPTIMIZATION OF STEAM CRACKING FURNACES

S.H. Symoens, M.R. Djokic, J. Zhang, G. Bellos, D. Jakobi, J. Weigandt, S. Klein,
F. Battin-Leclerc, G. Heynderickx, J. Van Thielen, B. Cuenot, T. Faravelli, G. Theis,
P. Lenain, A.E. Muñoz, J. Olver, K.M. Van Geem

2018 Spring National Meeting, Orlando, Florida, April, 24, 2018



ayming

business
performance
consulting





**GHENT
UNIVERSITY**

A SPIRE project



IMPROOF



POLITECNICO
DI MILANO



ayming

business
performance
consulting

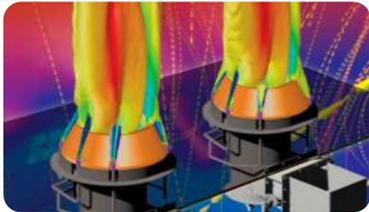


TechnipFMC

IMPROOF IS ALL ABOUT:

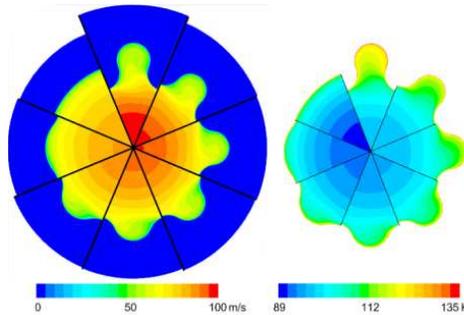
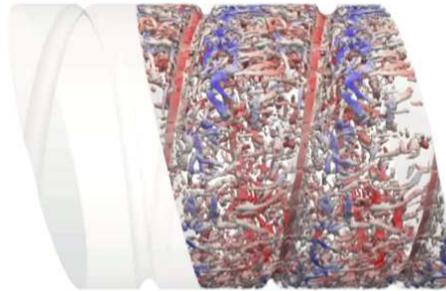
Renewable fuel characterization

- experimental activity
- kinetic mechanisms



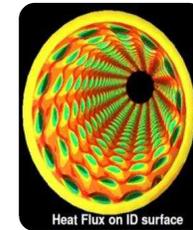
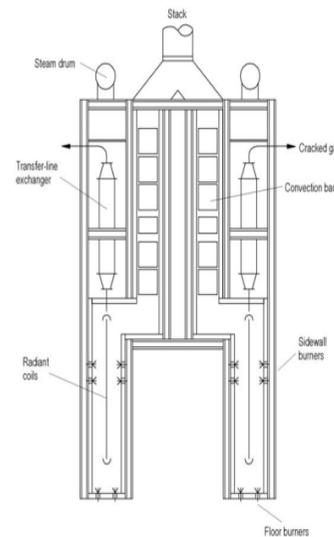
Advanced 3D modeling

- CFD RANS/LES
- Reactor optimization
- pilot plant simulation



Innovative Furnace System developments and integration

- oxy-fuel combustion
- emissivity coating
- coke formation
- 3D reactor testing



Upscaling and Demonstration



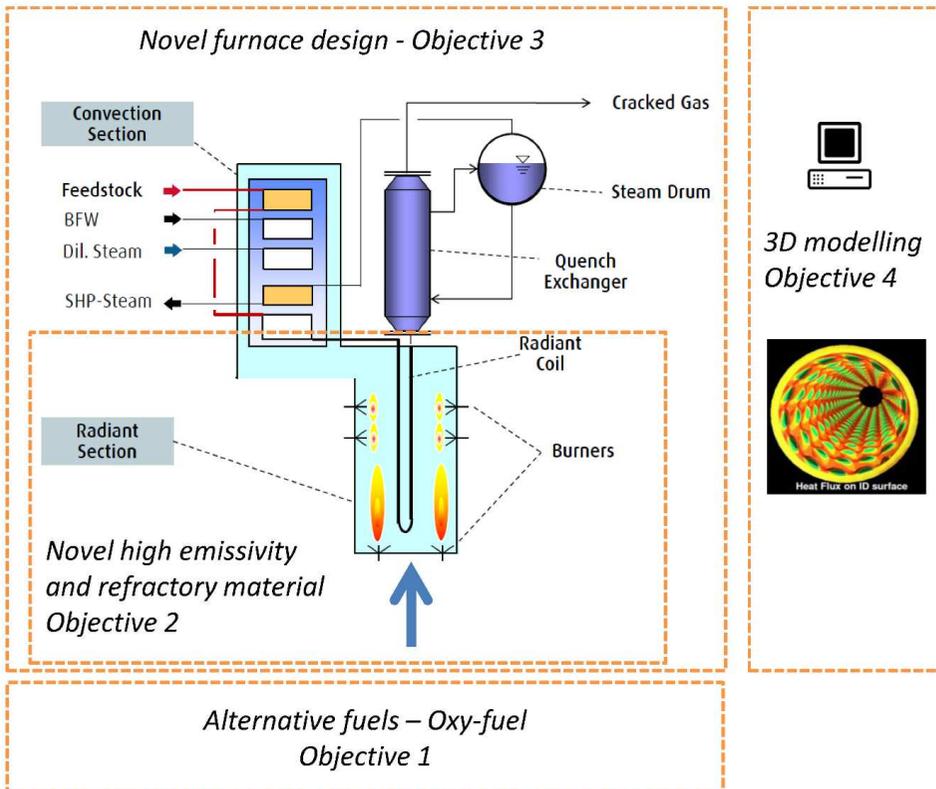
OUTLINE

- Introduction
- Objectives
- Coke formation on high-temperature alloys and 3D reactor technology
- Conclusions

OUTLINE

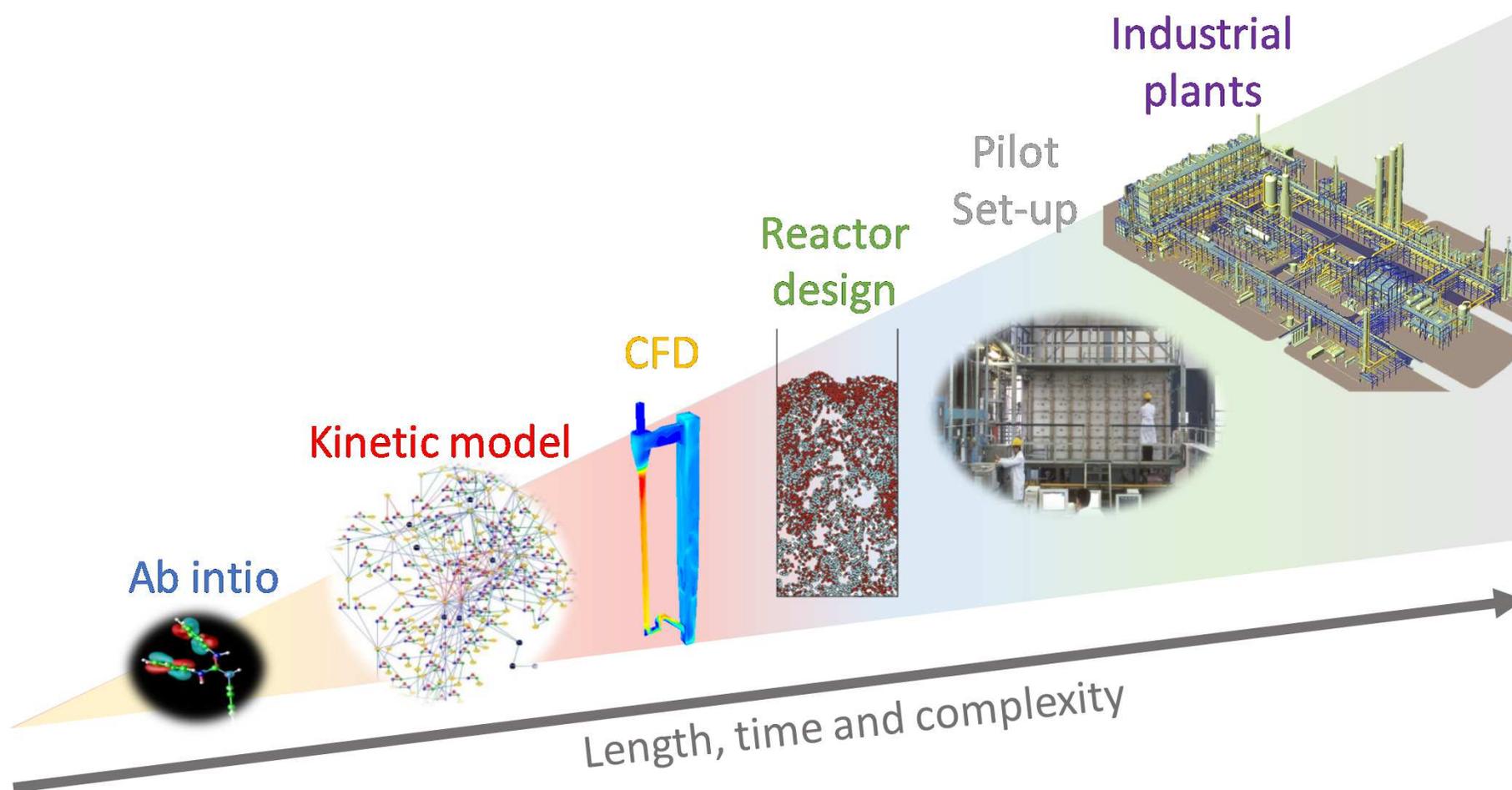
- Introduction
- **Objectives**
- Coke formation on high-temperature alloys and 3D reactor technology
- Conclusions

CONCEPT AND OBJECTIVES

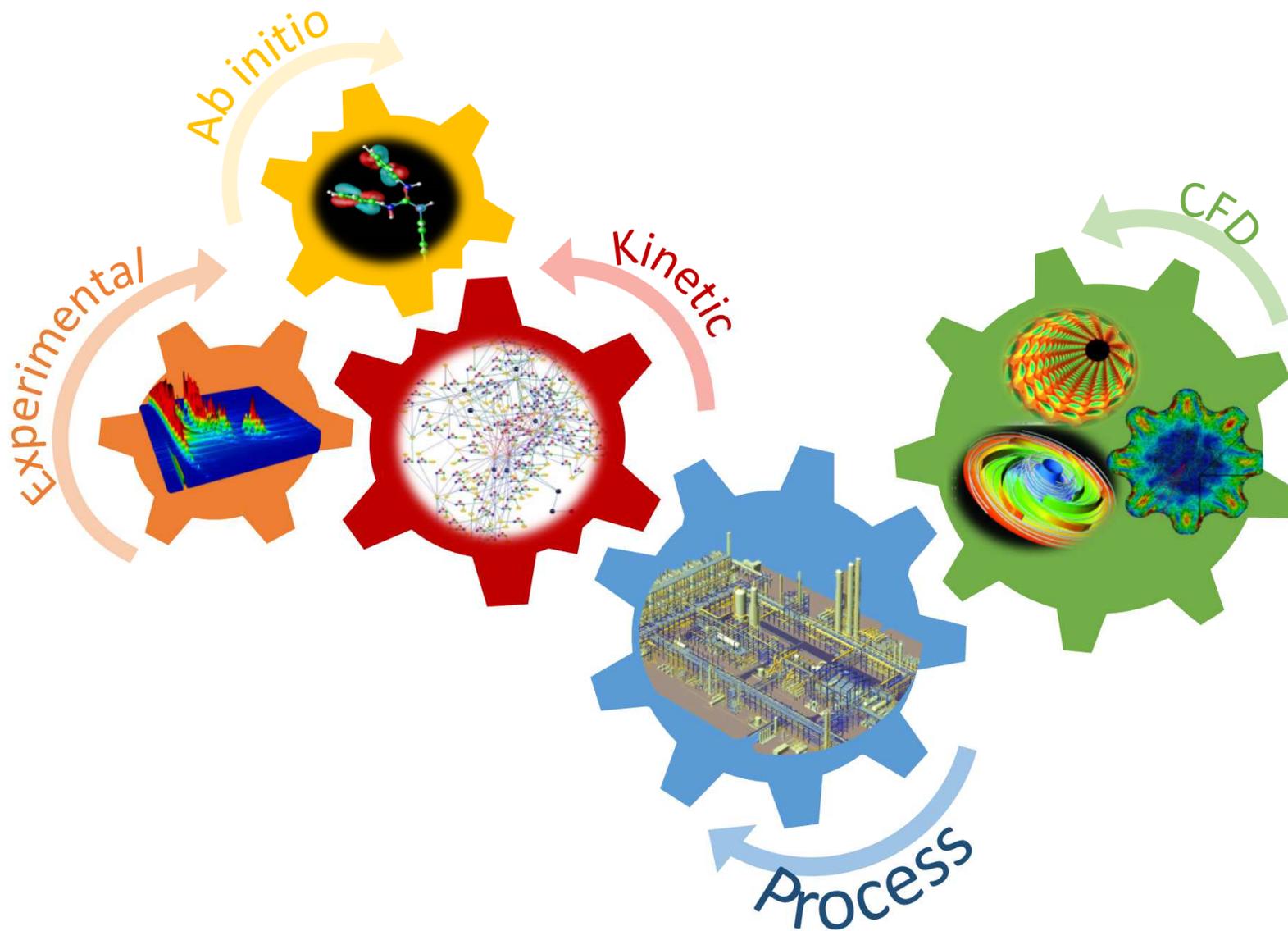


1. Novel combustion technology using alternative fuels and oxy-fuel combustion
2. Demonstrate the individual impact of **novel emissive, reactor and refractory materials on pilot scale (TRL5)**
3. Demonstrate the power of advanced process simulation (high performance computing and CFD) for furnace design and optimization
4. Demonstrate the technical economic and environmental sustainability of the IMPROOF furnace at TRL6
5. Coke formation reduction and real time optimization

MULTI SCALE APPROACH



LCT'S VISION



OUTLINE

- Introduction
- Objectives
- **Coke formation on high-temperature alloys and 3D reactor technology**
- Conclusions

COKE FORMATION

Deposition of a carbon layer on the reactor surface

- Thermal efficiency
- Product selectivity
- Decoking procedures



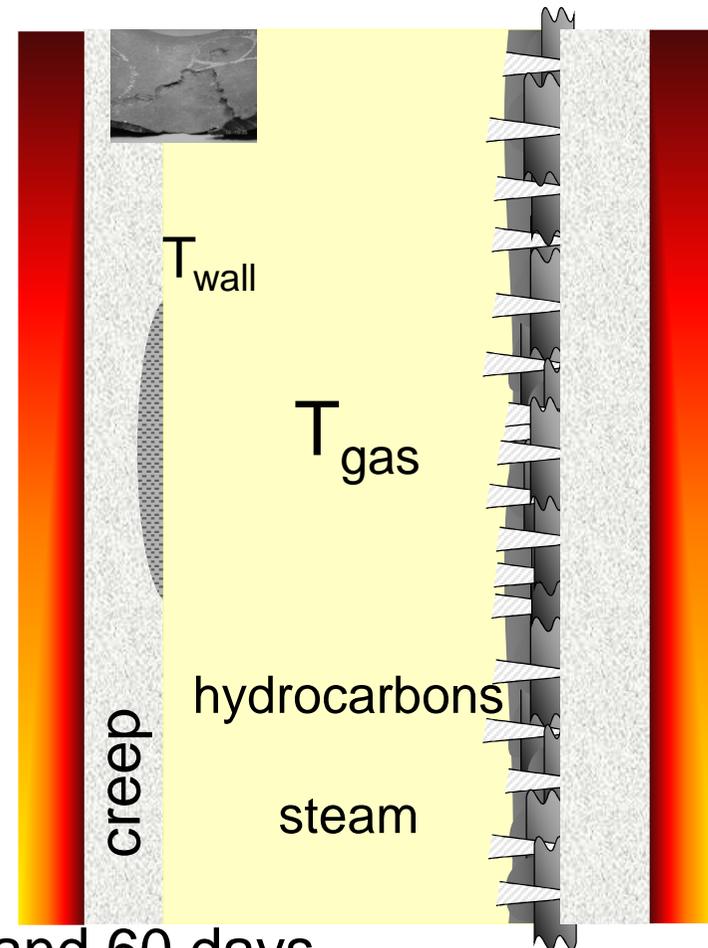
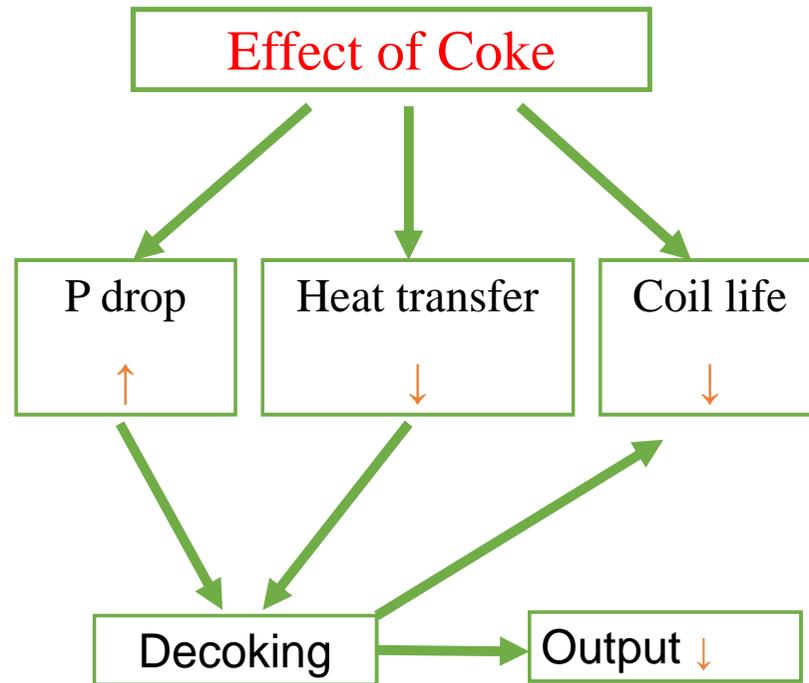
[Muñoz, 2013]

Estimated annual cost to industry: \$ 2 billion

Optimization by

- Feed additives
- Metallurgy & surface technology
- 3D reactor technology

COKES FORMATION



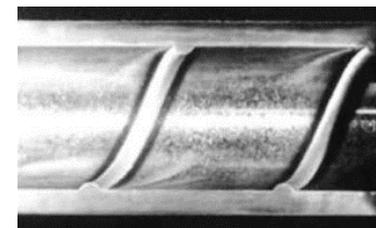
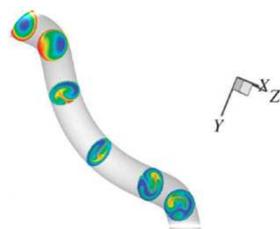
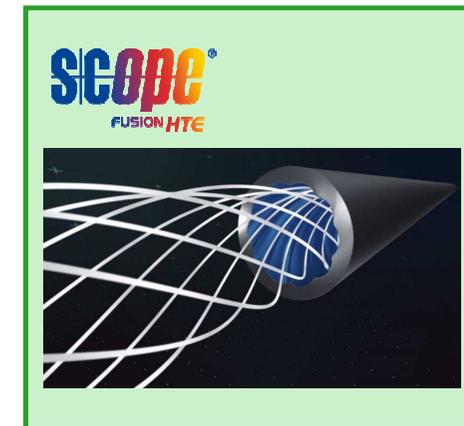
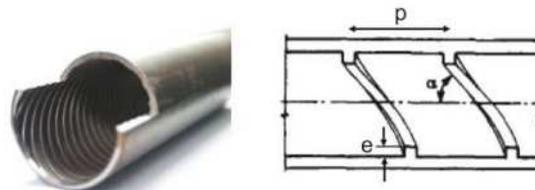
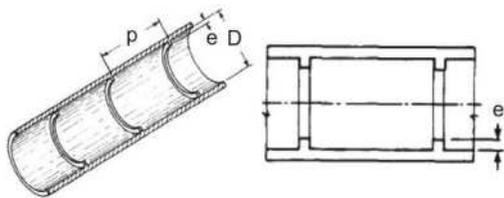
Run length is typically between 20 and 60 days

3D REACTOR TECHNOLOGY

Improve the reactor by decreasing $T_{\text{gas/coke}}$

$$Q = U \cdot A \cdot (T_{\text{gas/coke}} - T_{\text{bulk}})$$

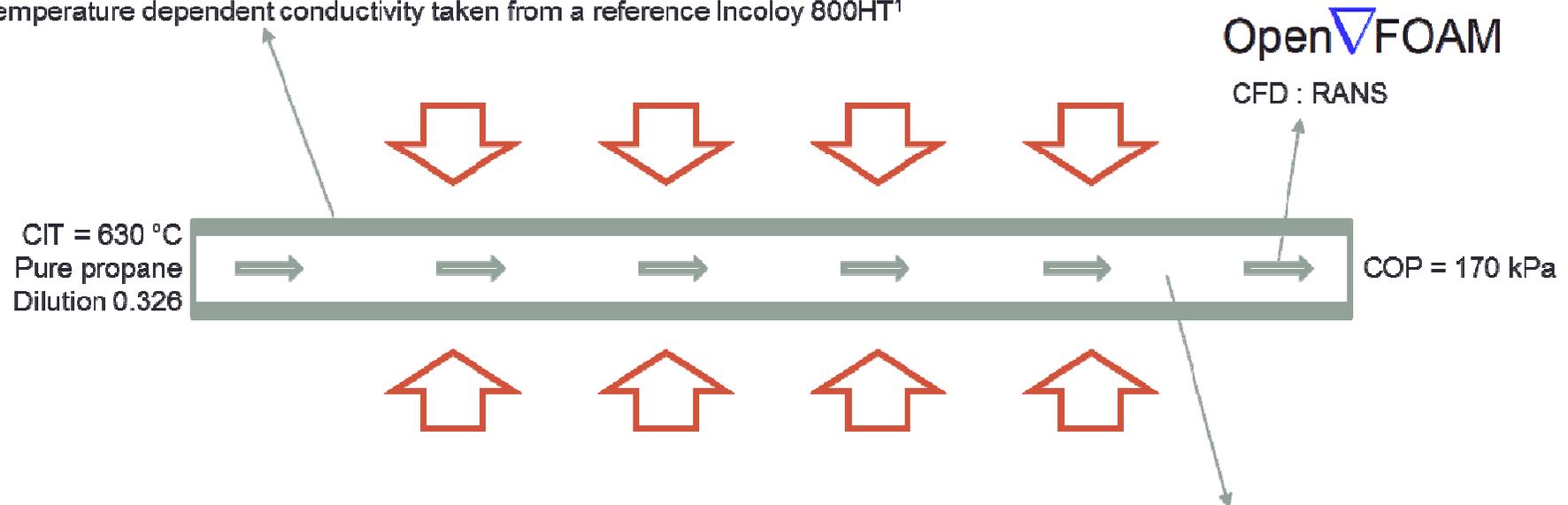
- Increase tube area (A)
- Increase heat transfer coefficient (U)



MILLISECOND BENCHMARK SIMULATION

Solving of the conjugated heat transfer: $\nabla \cdot (\lambda_g \nabla T) = 0$

Temperature dependent conductivity taken from a reference Incoloy 800HT¹



1D heat flux profile from furnace simulations
validated with industrial measurements

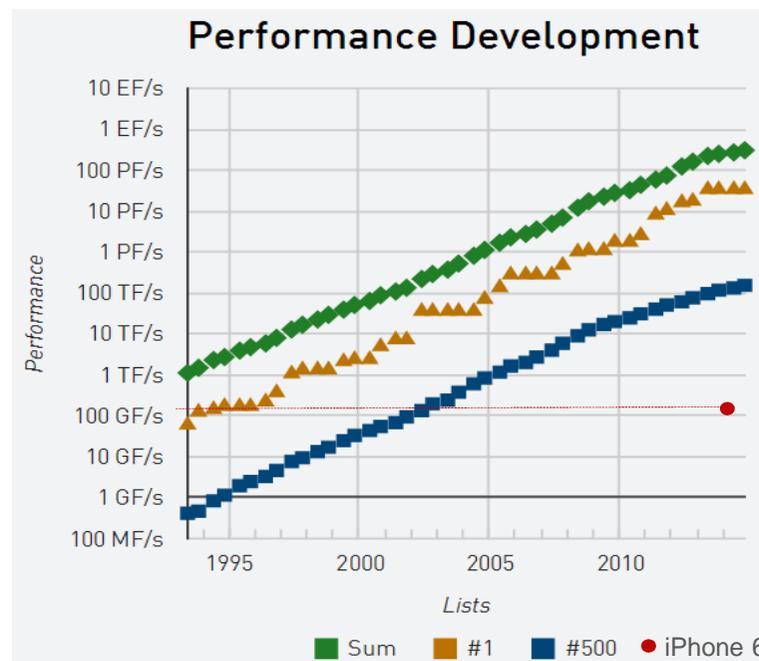
Linear scaling of heat flux profile to obtain
equal conversion for all reactor technologies

CRACKSIM model was reduced to its
relevant core for propane cracking.
Final network consists of 151 reactions
between 29 species of which 13 radical
species.
QSSA applied to reduce stiffness of the
model.⁹

SUPERCOMPUTING INFRASTRUCTURE



Tier-0 supercomputers

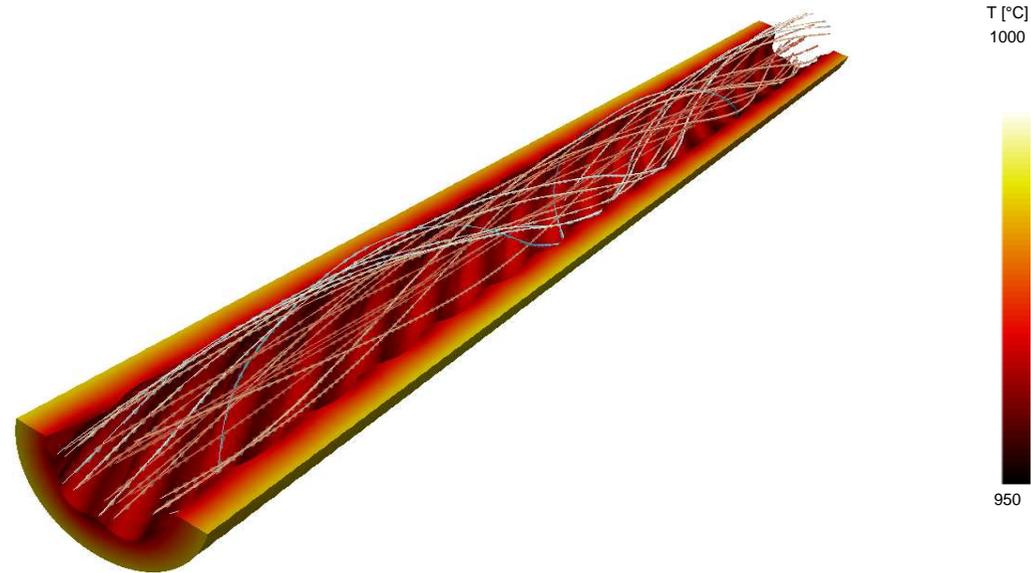


From \$15M world-record supercomputer to smartphone in 20 years

“SUPER” calculations are possible

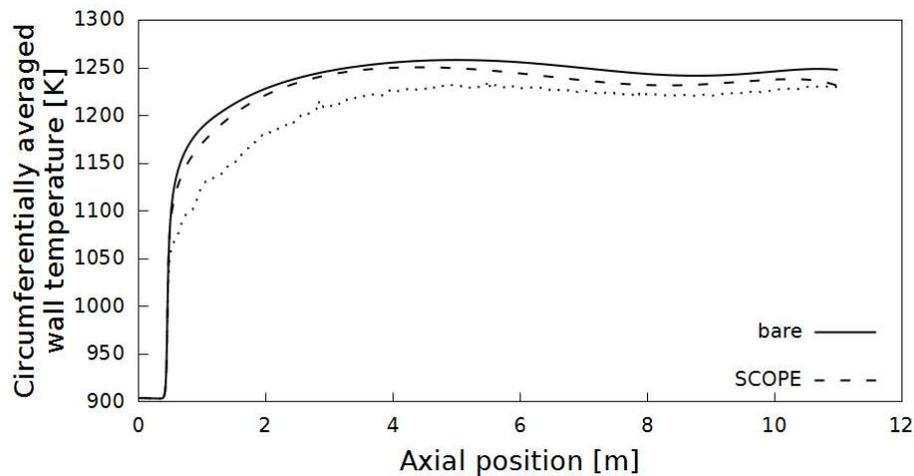
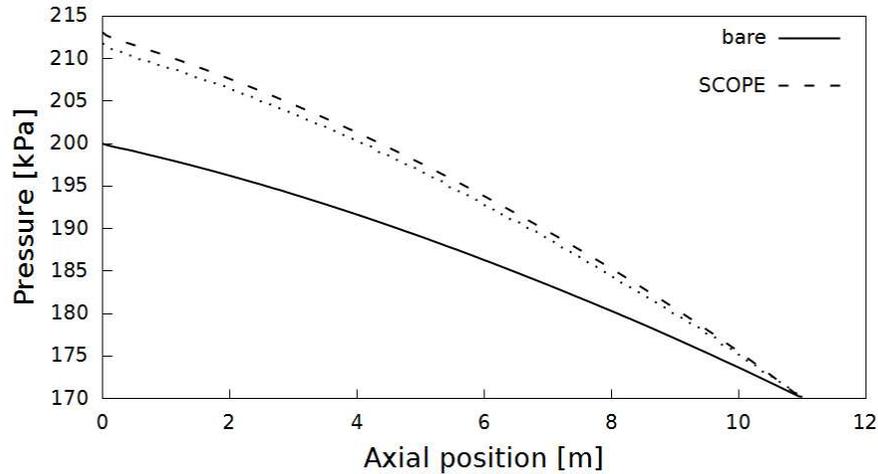
But are they useful?

COMPARISON TO BARE REACTOR



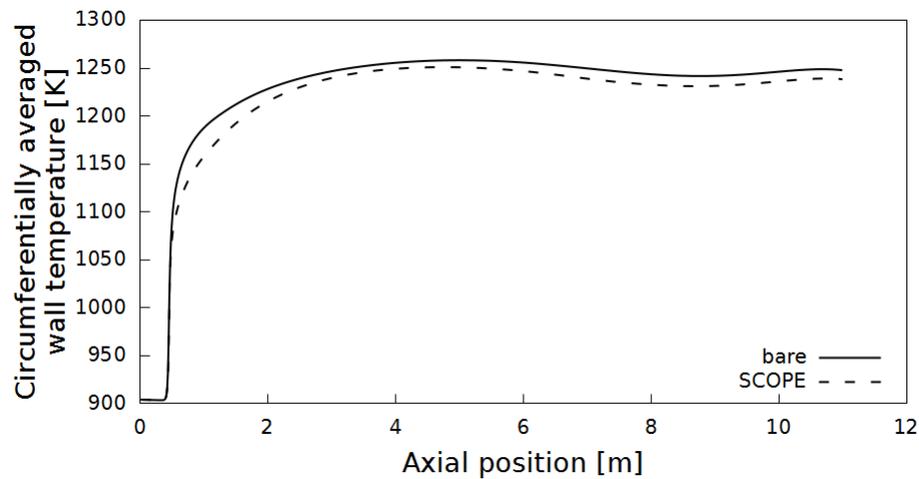
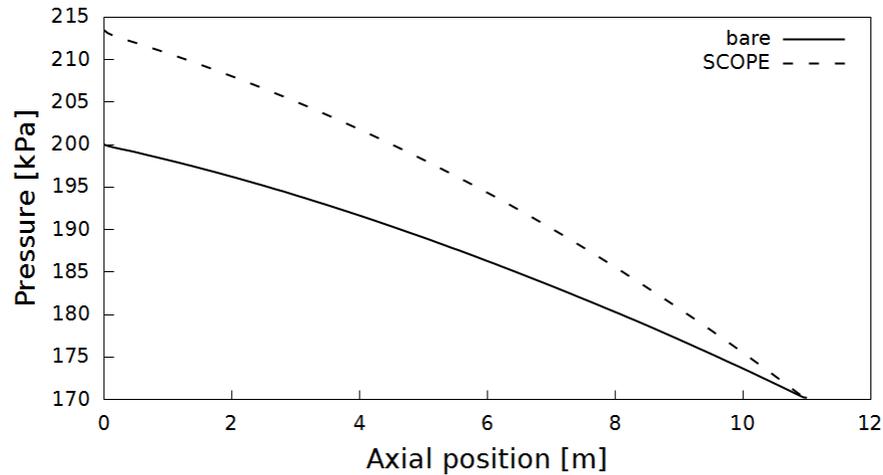
SCOPE	
976.7	TMT_{max} [°C]
1.40	$\Delta p/\Delta p_0$ [-]
1.006	$(P+E)/(P+E)_0$ [-]
0.536	P/E [-]

COMPARISON OF TECHNOLOGIES



		SCOPE
X	[%]	80.6
P/E	[-]	0.536
C ₂ H ₄	[wt%/wt ₀]	0.987
C ₃ H ₆	[wt%/wt ₀]	1.033
1-3.C ₄ H ₆	[wt%/wt ₀]	0.958
C ₂ H ₆	[wt%/wt ₀]	0.955
CH ₄	[wt%/wt ₀]	1.002
C ₂ H ₄	[wt%]	33.77
C ₃ H ₆	[wt%]	17.96
1-3.C ₄ H ₆	[wt%]	1.61
C ₂ H ₆	[wt%]	1.55
CH ₄	[wt%]	19.34

COMPARISON OF TECHNOLOGIES



		SCOPE
X	[%]	80.6
P/E	[-]	0.534
C ₂ H ₄	[wt%/wt% ₀]	0.985
C ₃ H ₆	[wt%/wt% ₀]	1.034
1-3.C ₄ H ₆	[wt%/wt% ₀]	0.953
C ₂ H ₆	[wt%/wt% ₀]	0.950
CH ₄	[wt%/wt% ₀]	1.000
C ₂ H ₄	[wt%]	33.70
C ₃ H ₆	[wt%]	17.99
1-3.C ₄ H ₆	[wt%]	1.60
C ₂ H ₆	[wt%]	1.54
CH ₄	[wt%]	19.30

SIMULATION ACCURACY GOOD ENOUGH?



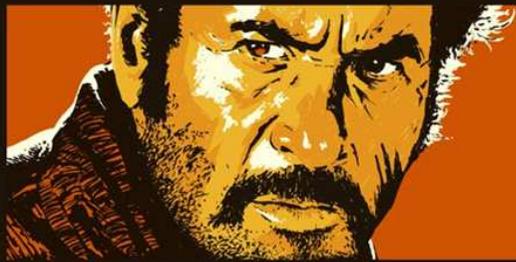
- **Burner geometry detail?**
- **Gas radiative properties?**
- **Furnace – Reactor coupling?**

3D REACTOR TECHNOLOGY



Enhanced heat transfer & mixing -> Less cokes?

Increased pressure drop
Lower olefin selectivity?



Long term performance and stability?

REACTORS

Centralloy® ET 45 Micro

Centralloy® HT E

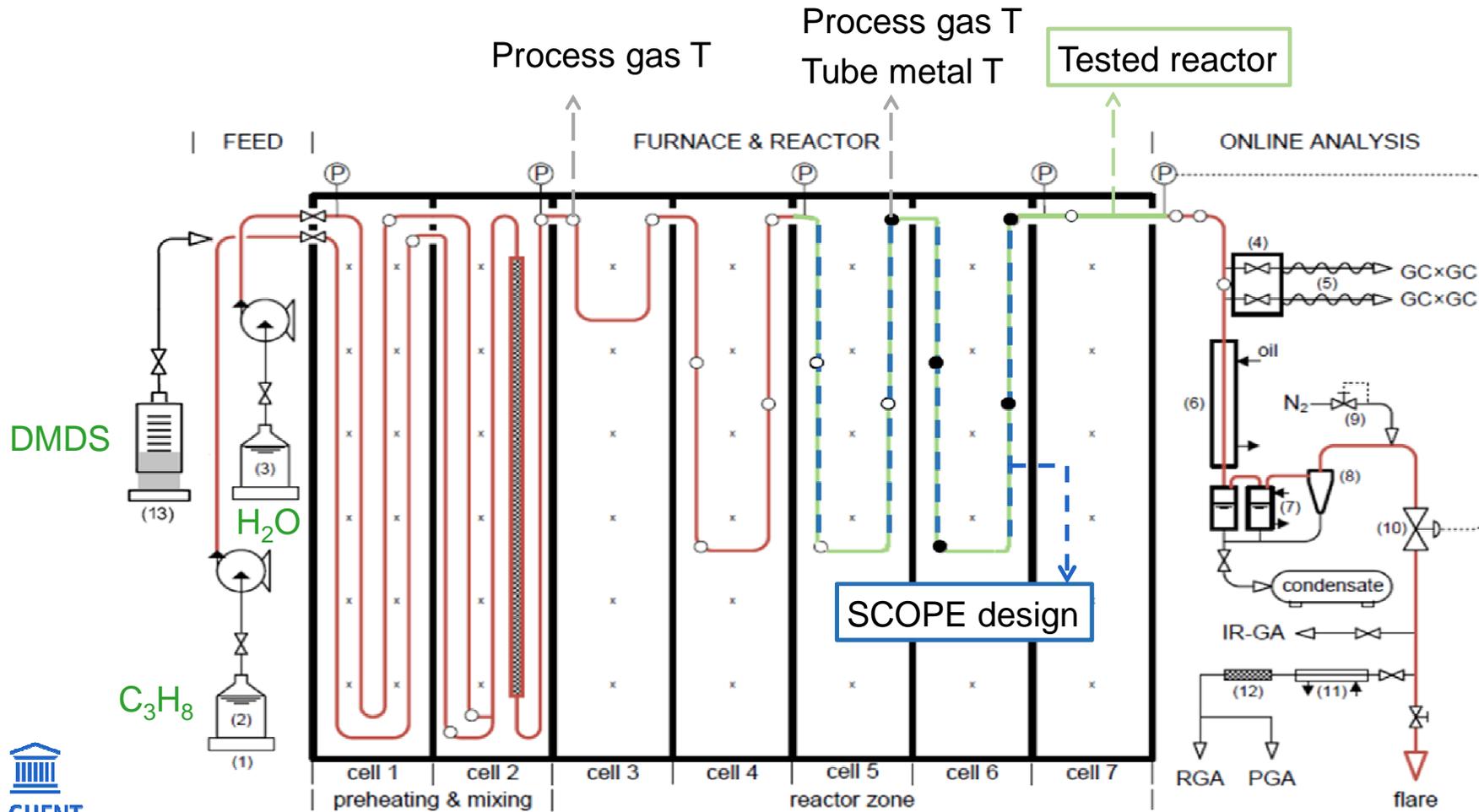
Centralloy® HT E + SCOPE®



Alloy	Composition [wt %]								Additions
	C	Si	Mn	Cr	Fe	Ni	Al	Nb	
ET 45 Micro	0.45	1.6	1.0	35	bal.	45	-	1.0	MAE, RE
HT E	0.45	-	-	30	bal.	45	4.0	0.5	MAE, RE

RE: reactive elements; MAE: micro-alloying elements

PILOT PLANT



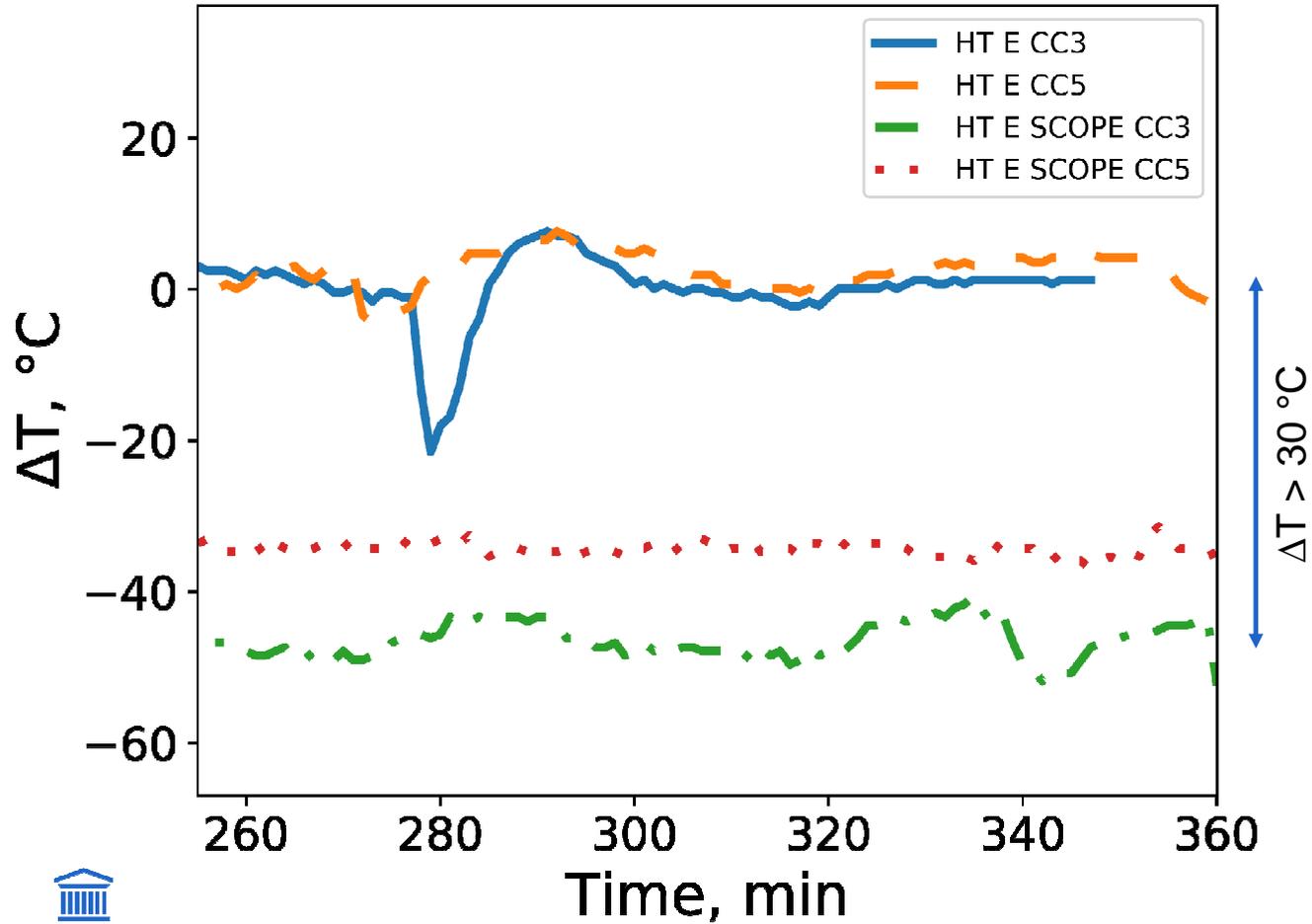
EXPERIMENTAL PROGRAM

- Steam treatment for 10 hours
- 1CC: COT = base; 6 hours
- 2CC: COT = base; 2 hours
- 3CC: COT = base; 6 hours
- 4CC: COT = base + 110 °C/ + 160 °C*; 1.67 hours
- 5CC: COT = base; 12 hours

*SCOPE®

- ✓ Decoking was performed after every Cracking Cycle (CC)
- ✓ Prior to each CC a pre-sulfiding step was performed

TUBE METAL TEMPERATURES



Pyrometer

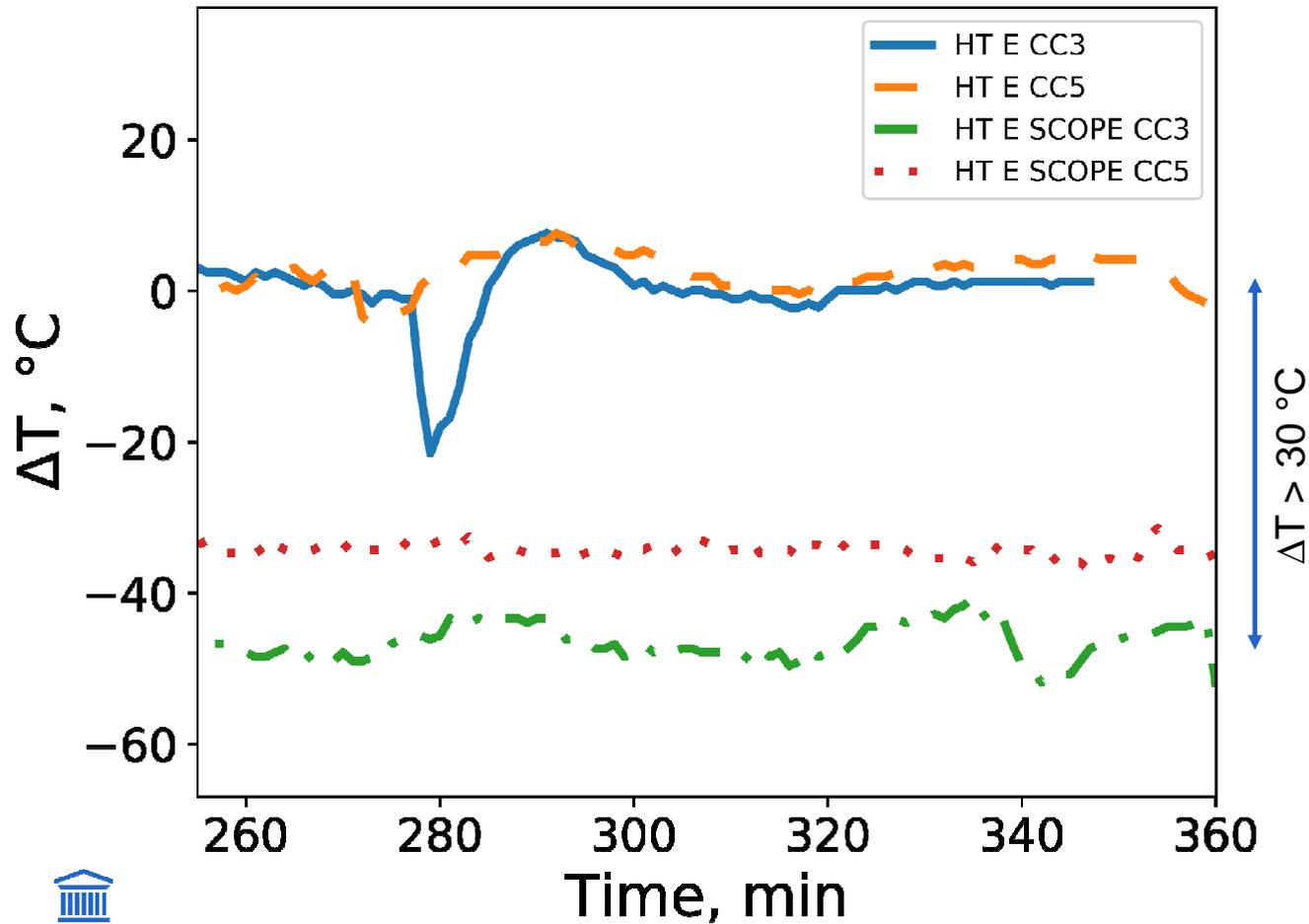


Manual T



Weld-on TC's

TUBE METAL TEMPERATURES

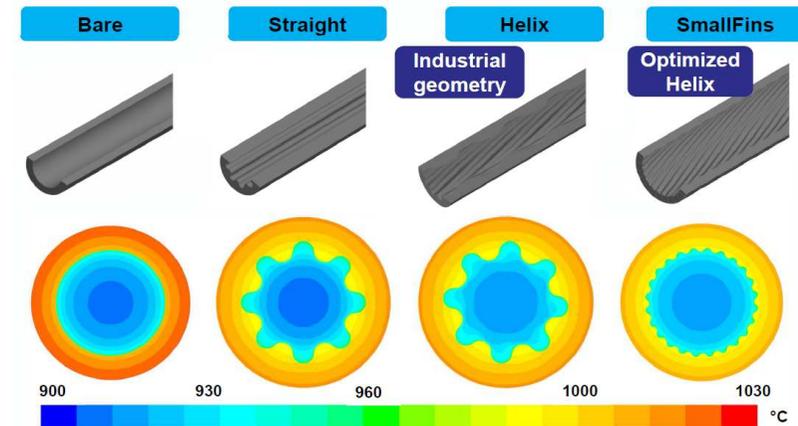


Gas consumption



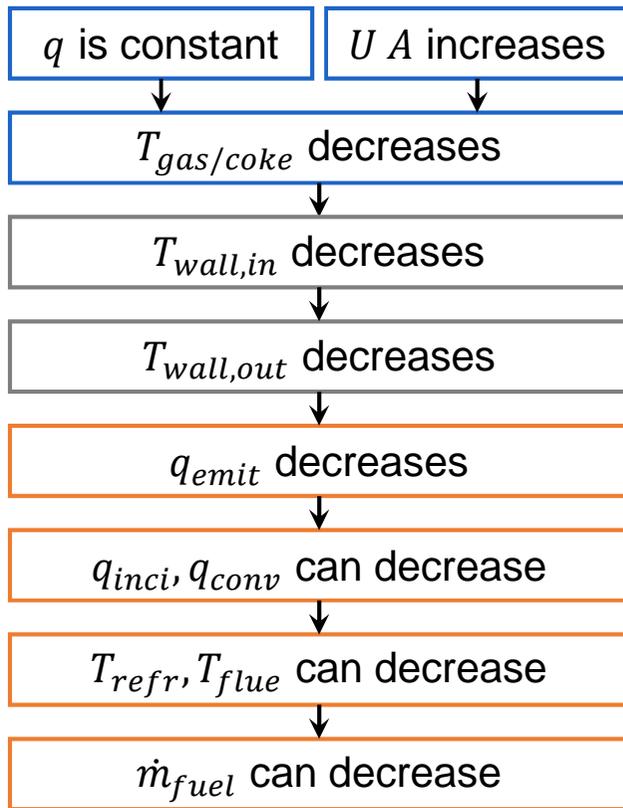
Result

~10 % lower
Fuel gas consumption



TUBE METAL TEMPERATURES

30°C lower tube metal temperature reduces fuel consumption by ~10%



Convection on inner wall

$$q = U A (T_{gas/coke} - T_{bulk})$$

Conduction through coke

$$q = k_c A (T_{wall,in} - T_{gas/coke}) / d_c$$

Conduction through metal

$$q = k_m A (T_{wall,out} - T_{wall,in}) / d_m$$

Heat balance on outer wall

$$q = [q_{inci} - q_{re} + q_{conv}] - q_{emit}$$

$$\varepsilon_w q_{inci} + q_{conv}$$

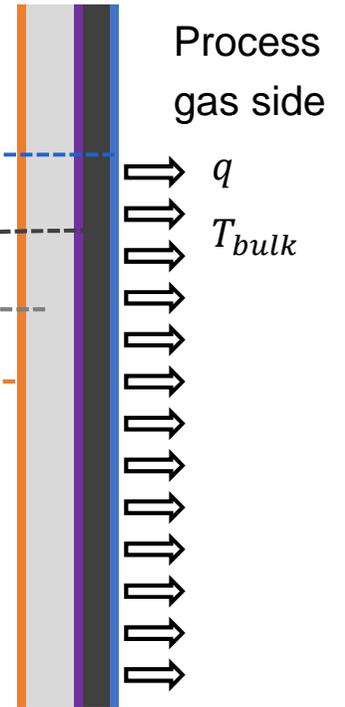
$$\varepsilon_w \sigma T_{wall,out}^4$$

$$\sim T_{refr}, T_{flue}$$

$$\sim \dot{m}_{fuel}$$

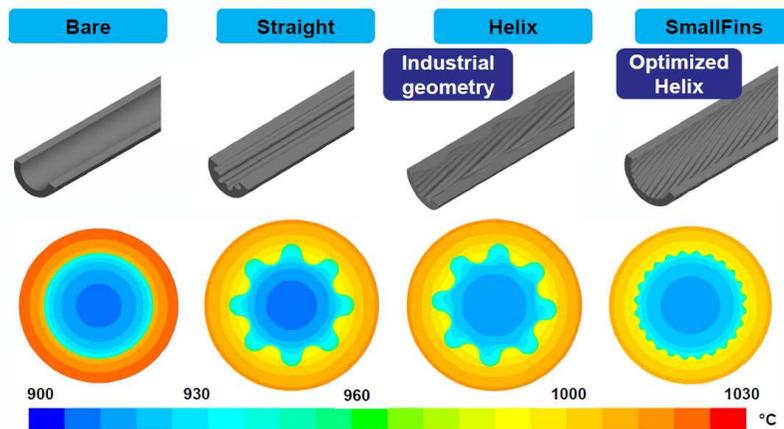
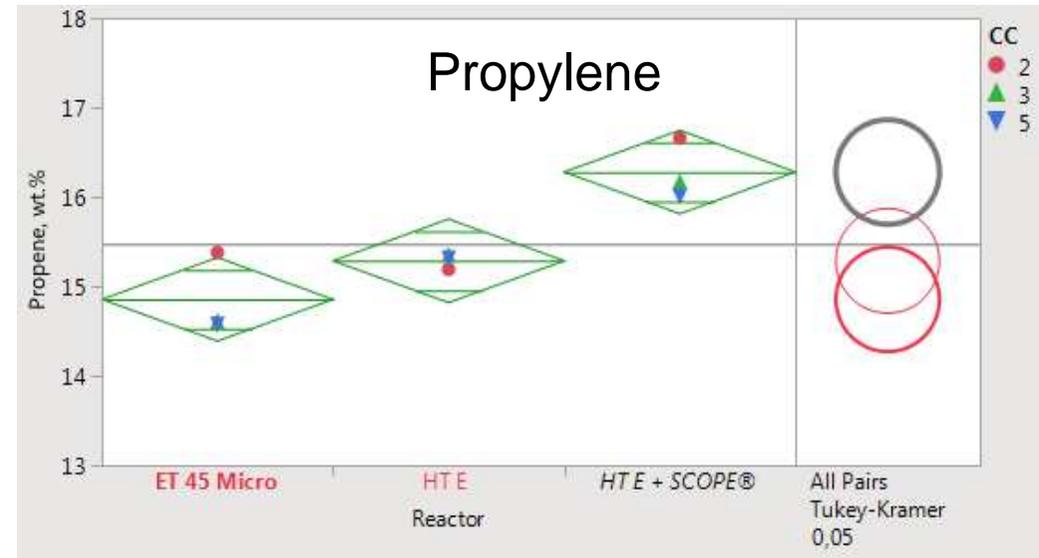
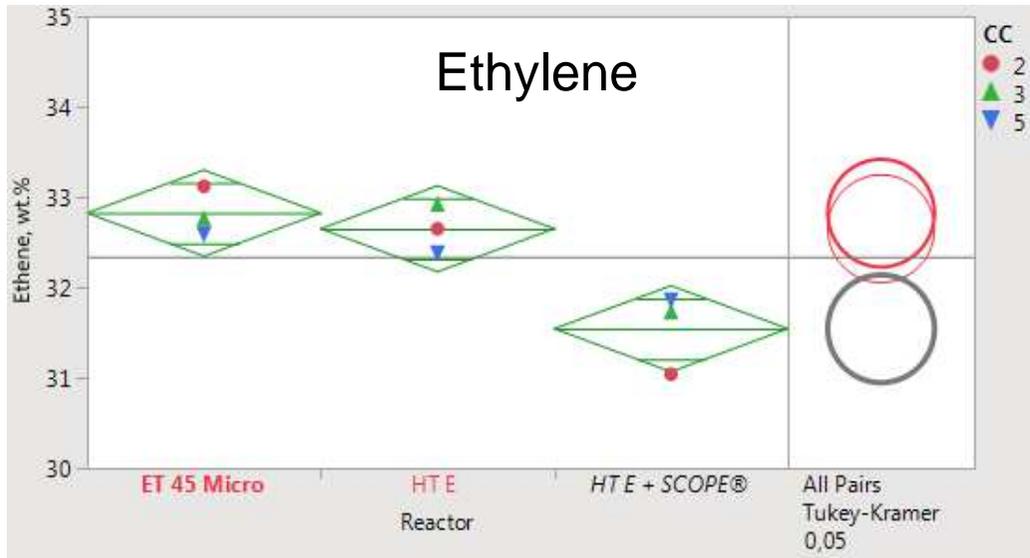
Flue gas side

Process gas side



PRODUCT YIELDS

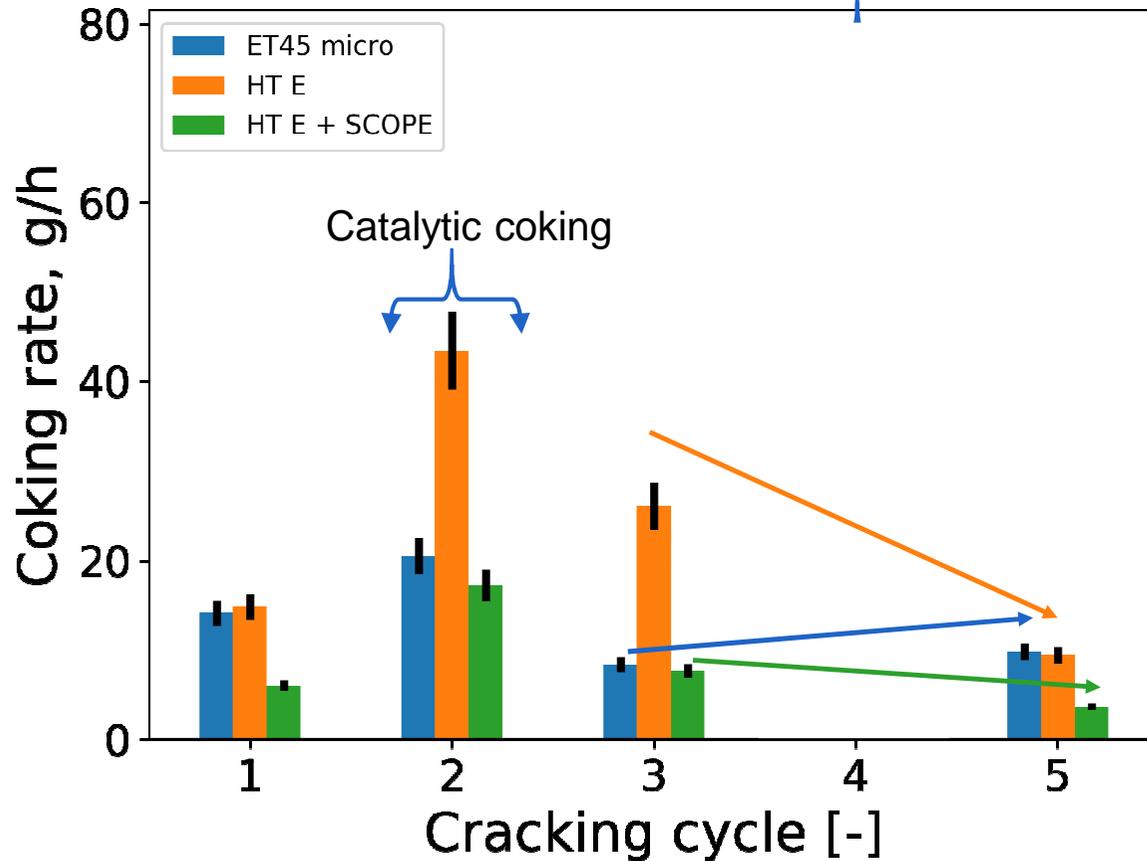
2 (CC2), 6 (CC3) and 12 h (CC5) cracking cycles



Reduced over-cracking near wall

COKING RATES

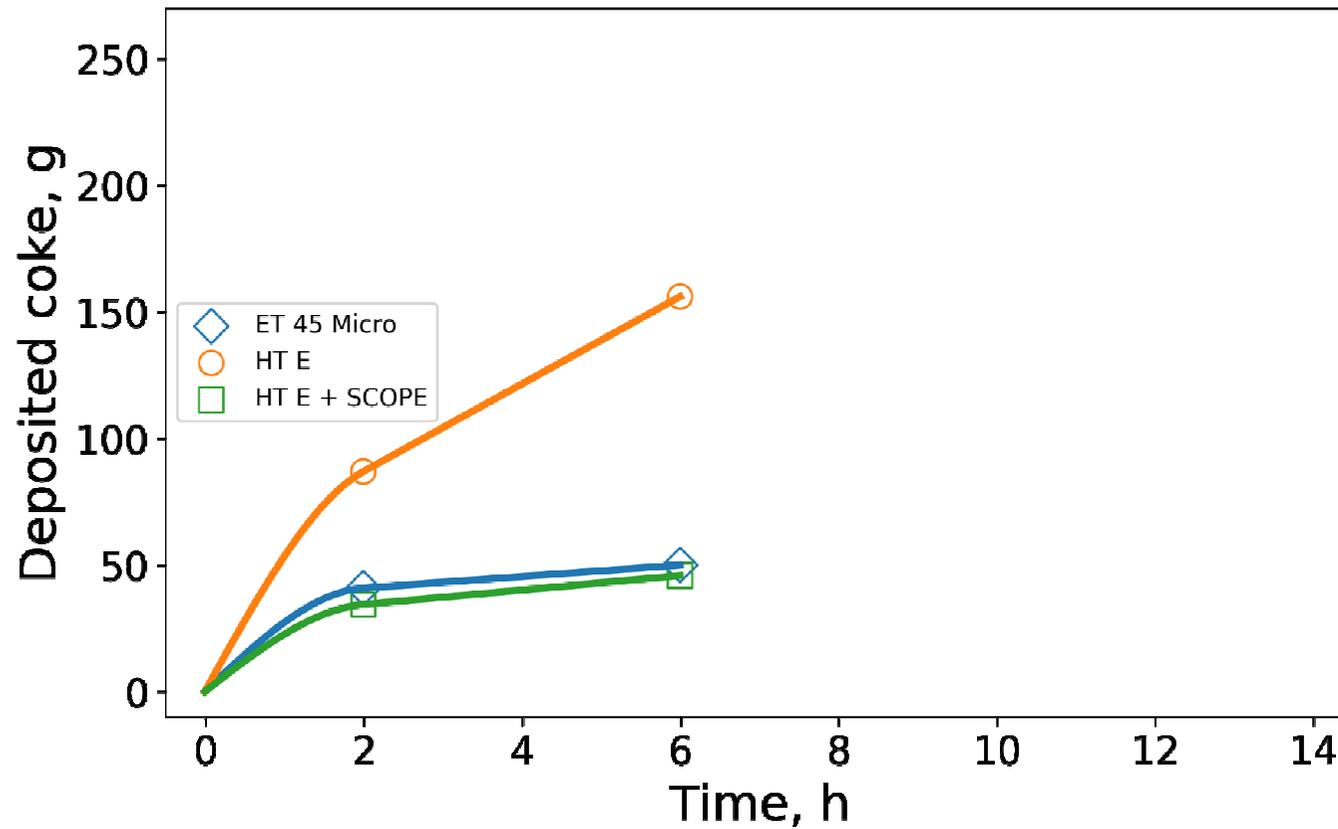
High T (EOR)



- 1CC: COT; 6 hours
- 2CC: COT; 2 hours
- 3CC: COT; 6 hours
- 4CC: COT+110 °C/+160 °C*; 1.67 hours
- 5CC: COT = base; 12 hours
- *SCOPE

- Increase after high T exp
- Reduction after high T exp
- Reduction after high T exp

COKE DEPOSITION



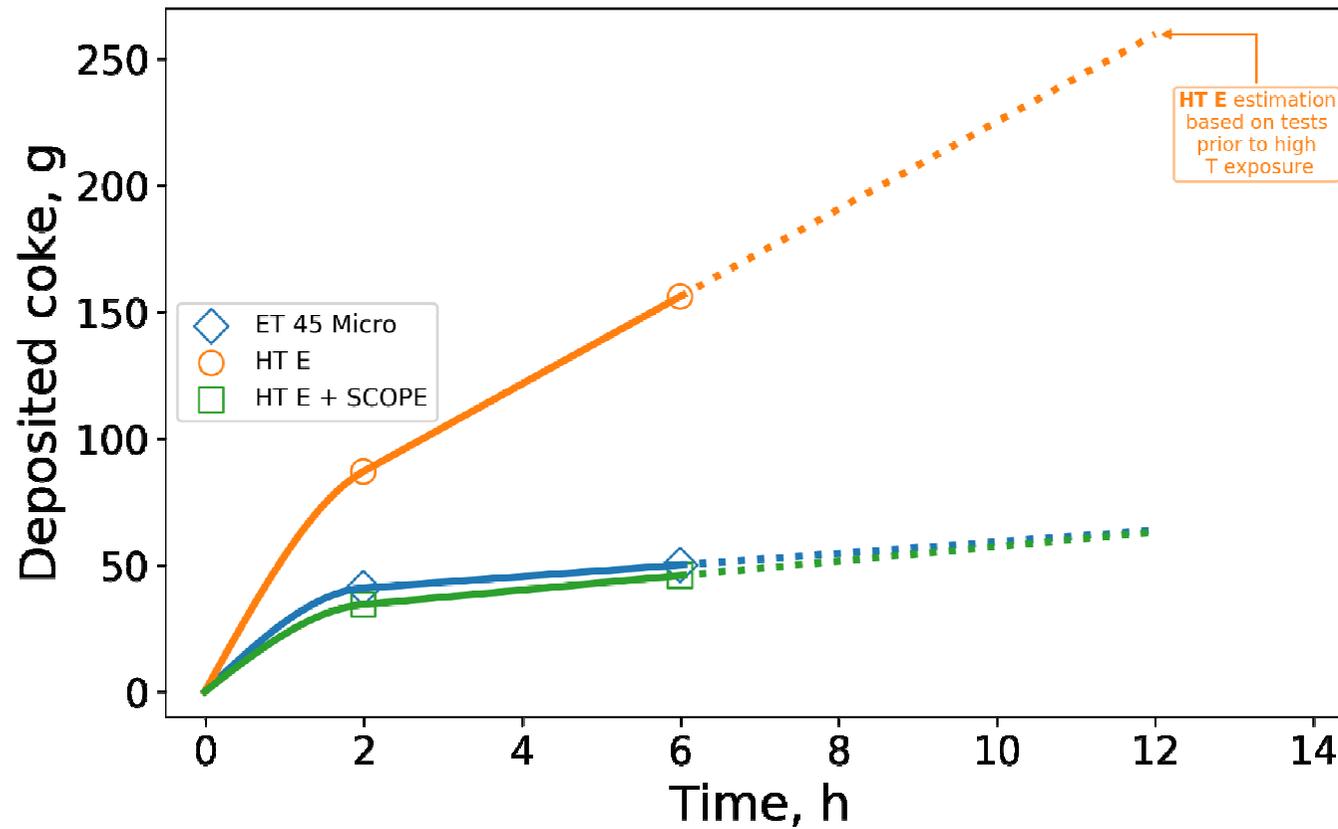
Coke after 2 (CC2) and 6h (CC3)

ET 45 Micro and HT E + SCOPE
comparable

HT E significantly worse

Line: estimated coking curve

COKE DEPOSITION



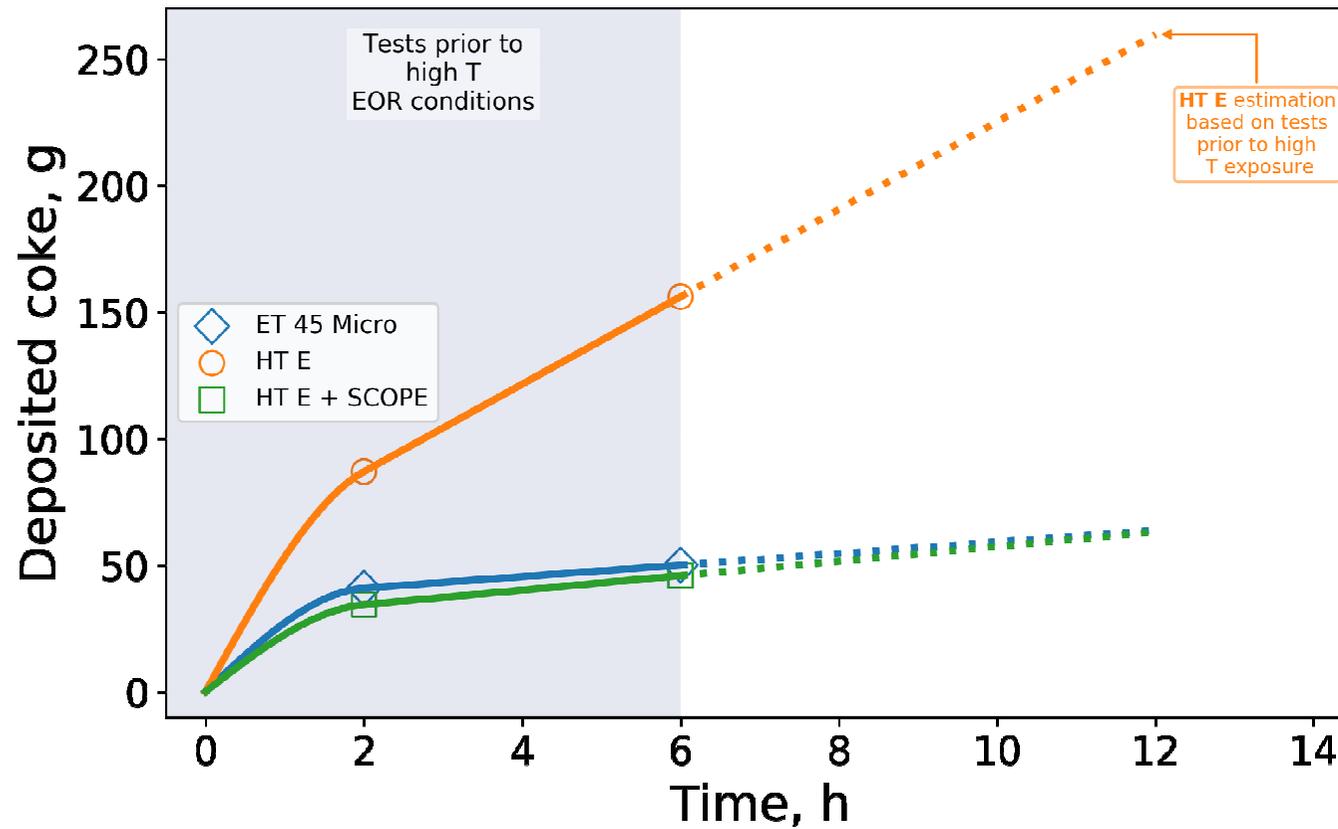
Extrapolation for 12 h coke

Assumptions:

2 h (CC2) = Catalytic

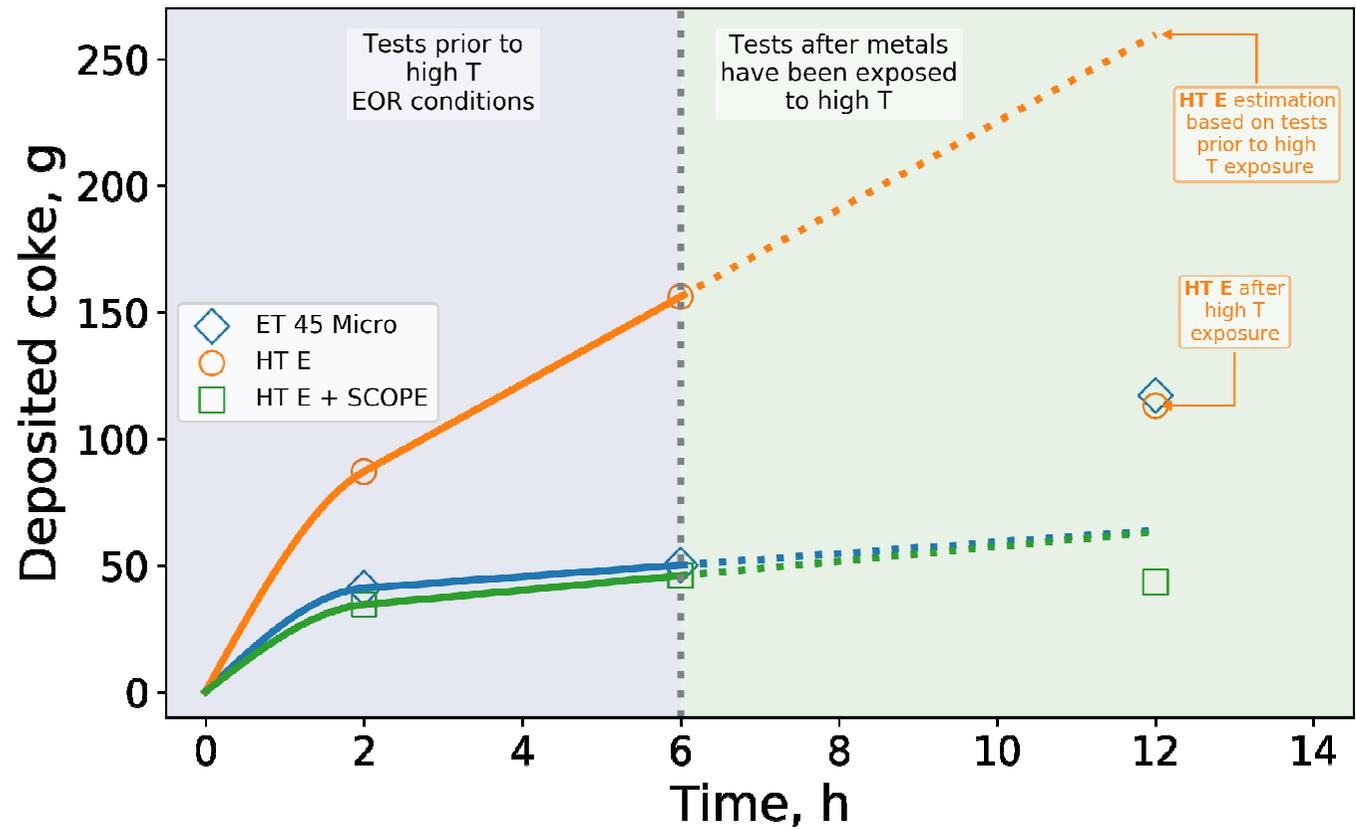
6 h (CC3) = asymptotic

COKE DEPOSITION



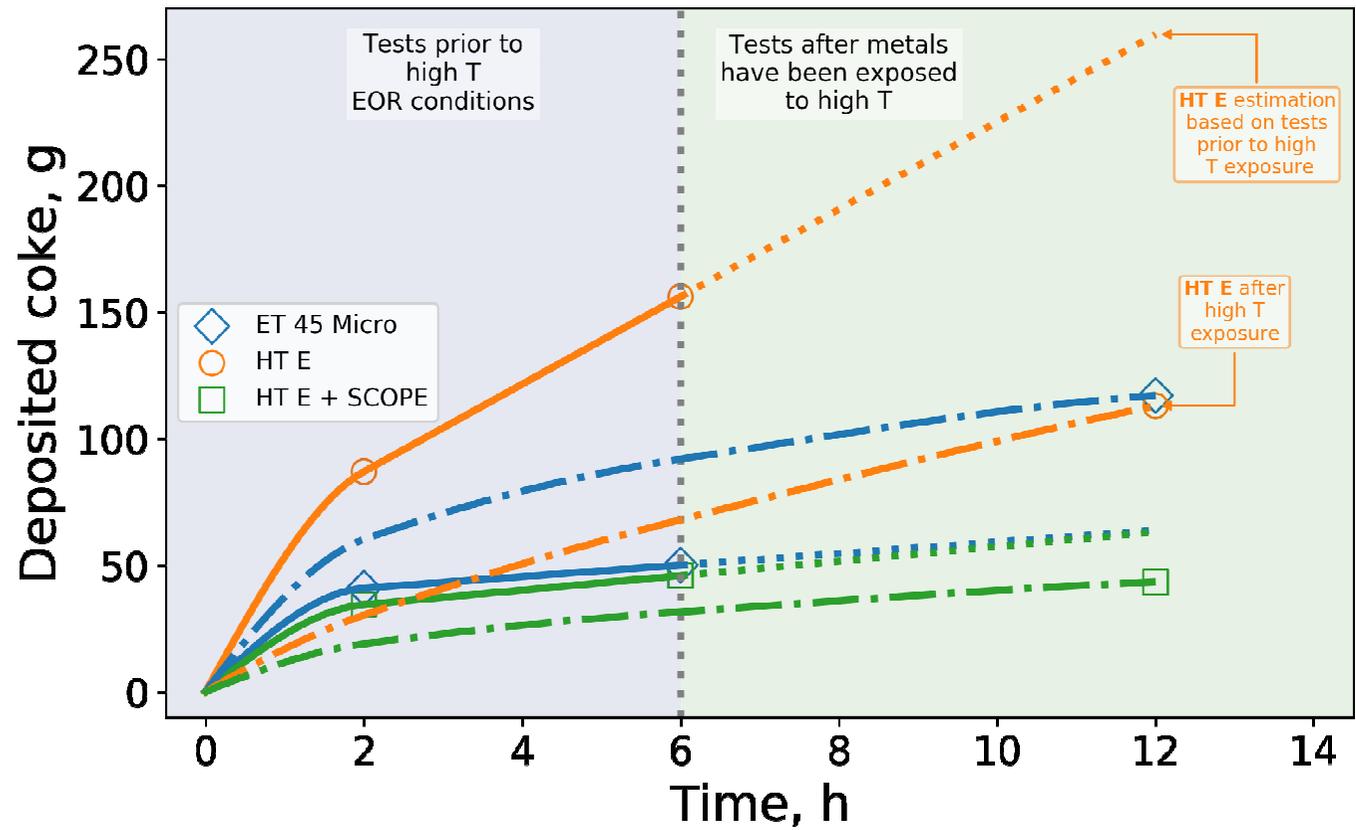
Extrapolation based on tests prior to high T (EOR) exposure

COKE DEPOSITION



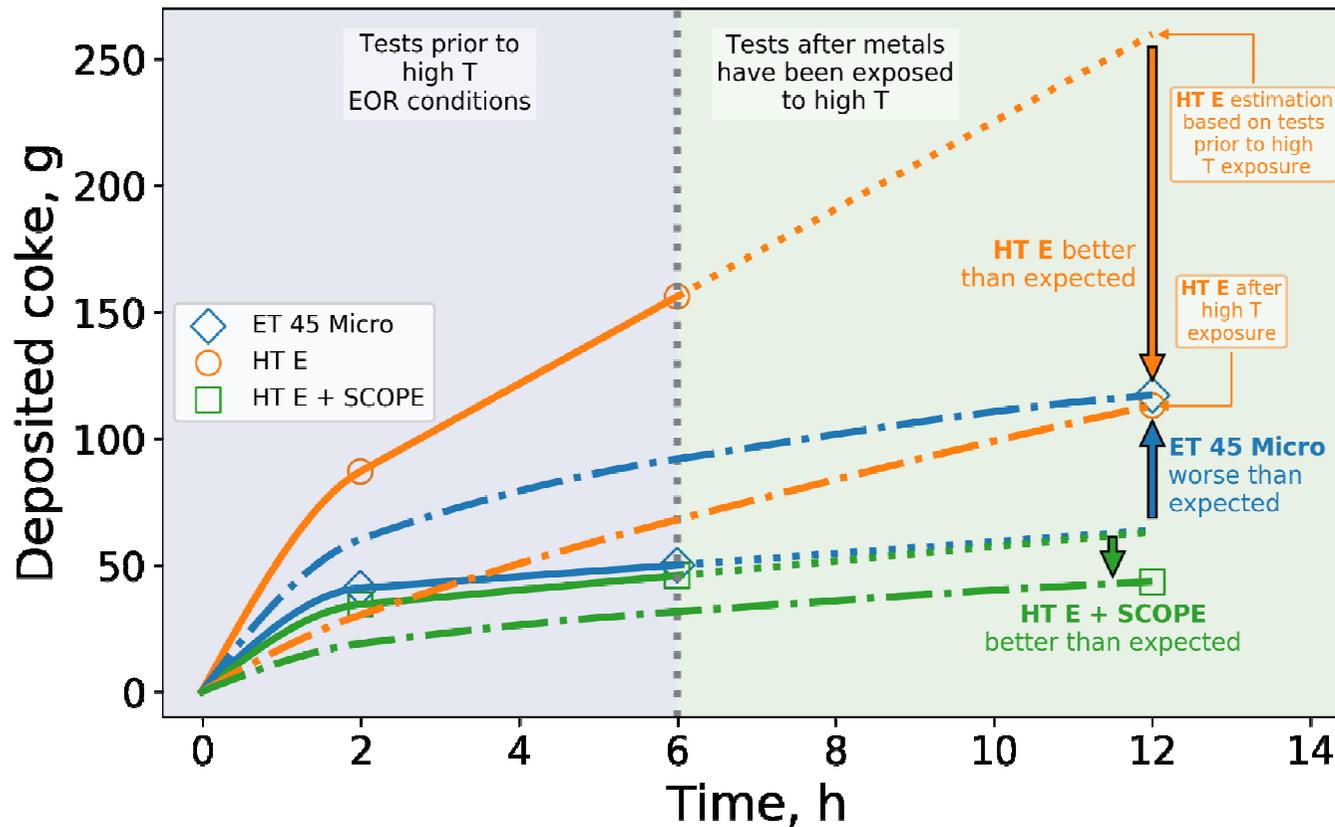
Coke after high T exposure

COKE DEPOSITION



Estimation coking curve

COKE DEPOSITION

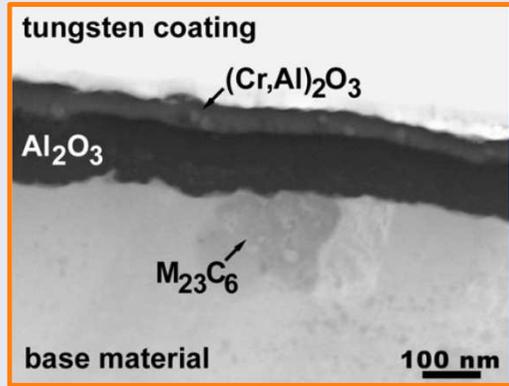


HT E better than expected

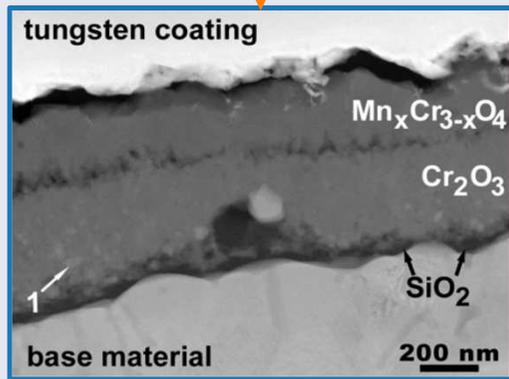
ET 45 Micro worse than expected

SCOPE design →
 Lower temperatures
 Lower influence high T excursion

COKE DEPOSITION

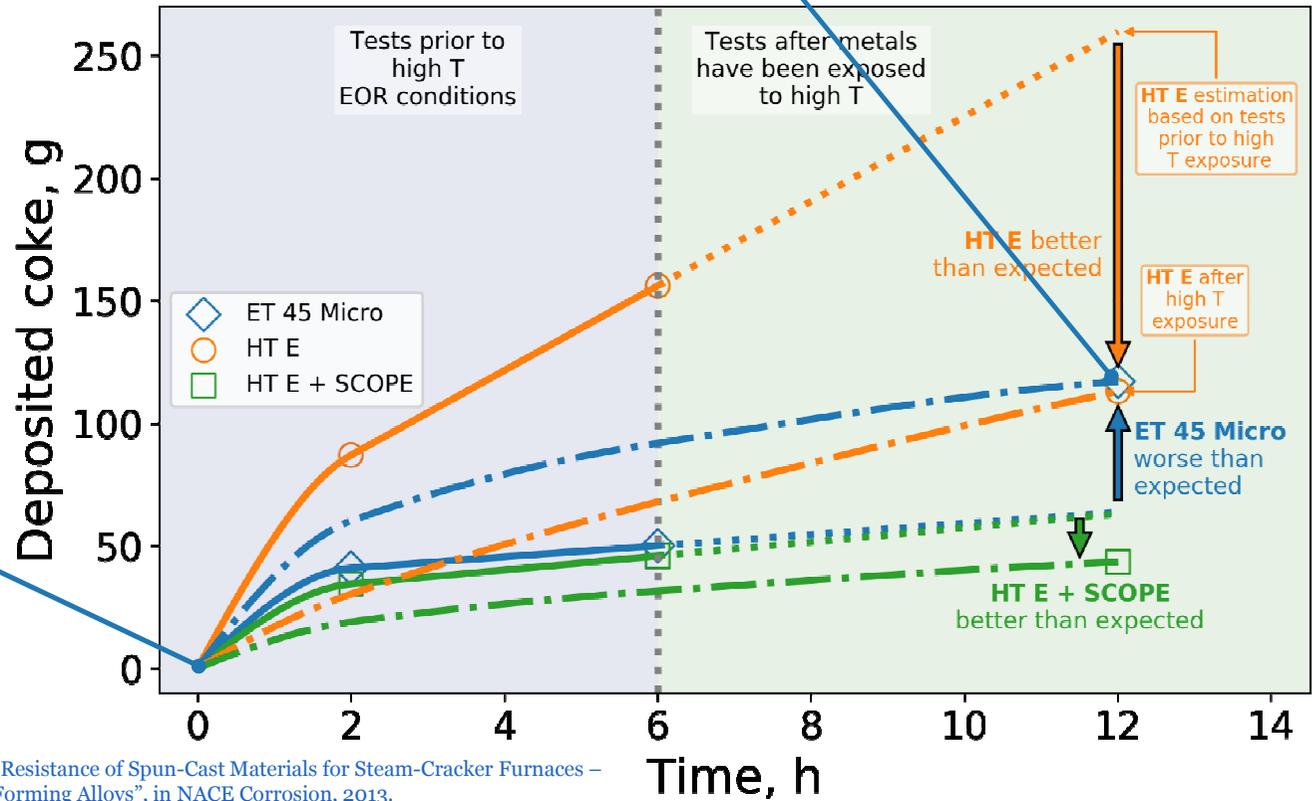
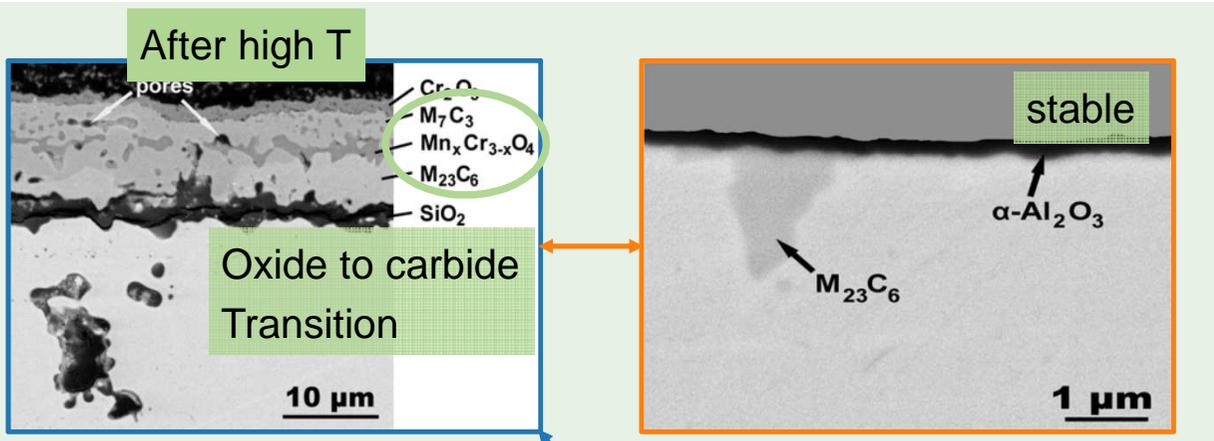


HT E

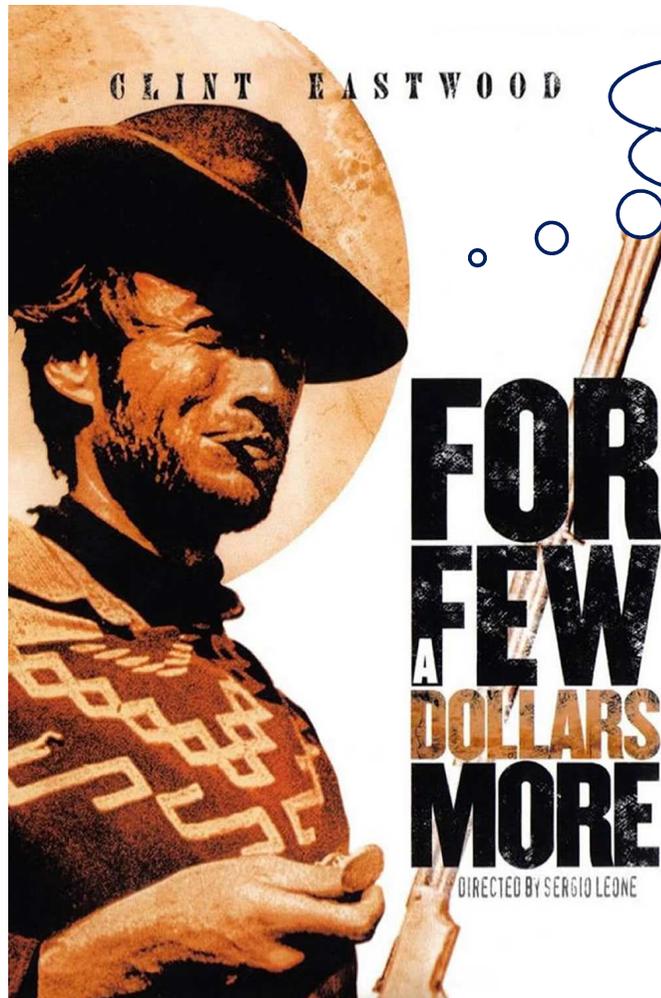


ET 45 Micro

After pre-Ox
Before high T



FOR A FEW DOLLARS MORE



Cracking furnace under
**optimal operating
conditions**

- Safety
- Production
- Emission
- Energy efficiency
- Run length

NEXT STEPS

- Testing high emissivity coating's performance in the **pilot plant** furnace/cracker at UGent at TRL5 level
 - benchmark to uncoated ethylene furnace by calculating the thermal efficiency of the improved furnace
- Comparison SCOPE[®] vs bare in reactive 3D CFD simulations

OUTLINE

- Introduction
- Objectives
- Coke formation on high-temperature alloys and 3D reactor technology
- **Conclusions**

CONCLUSIONS

- After high Temperature (EOR) exposure **HT E** performs **better**, while the performance of **ET 45 Micro drops**
- **ET 45 Micro** → Oxide to carbide transition
- **HT E** → Formation stable $\alpha\text{-Al}_2\text{O}_3$ scale
- Combining the advanced coil material (**HT E**) and novel 3D reactor design (**SCOPE[®]**) leads to
 - Increased run lengths
 - Improved product selectivities
 - Longer lifetime of the reactor coils
 - Higher energy efficiency of the furnace

ACKNOWLEDGMENT

- The work leading to this intervention has received funding from the European Union H2020 (H2020-SPIRE-04-2016) under grant agreement n°723706 and from the COST Action CM1404 “Chemistry of smart energy carriers and technologies”.

Thank you for your attention!



GLOSSARY

- CC: Cracking cycle
- DMDS: dimethyl disulfide
- CFD: computational fluid dynamics
- RE: reactive elements
- MAE: micro-alloying elements
- RGA: refinery gas analyzer
- IR GA: infrared analyzer
- PGA: permanent gas analyzer
- COT: coil outlet temperature
- TMT: Tube metal temperature

Kevin M. Van Geem

Full Professor

LABORATORY FOR CHEMICAL TECHNOLOGY

E Kevin.VanGeem@ugent.be

T +32 9 264 55 97

M +32 478 57 38 74

www.ugent.be

 Ghent University

 @ugent

 Ghent University