

Computational Fluid Dynamics-based Study of the Steam Cracking Process using a Hybrid 3D-1D Approach

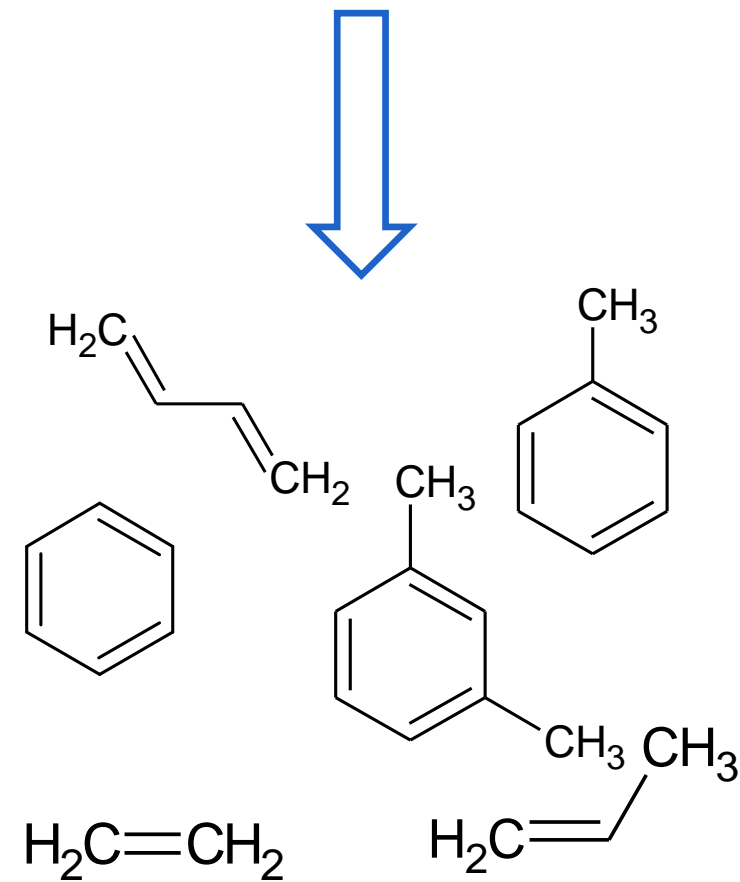
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¹Laboratory for Chemical Technology

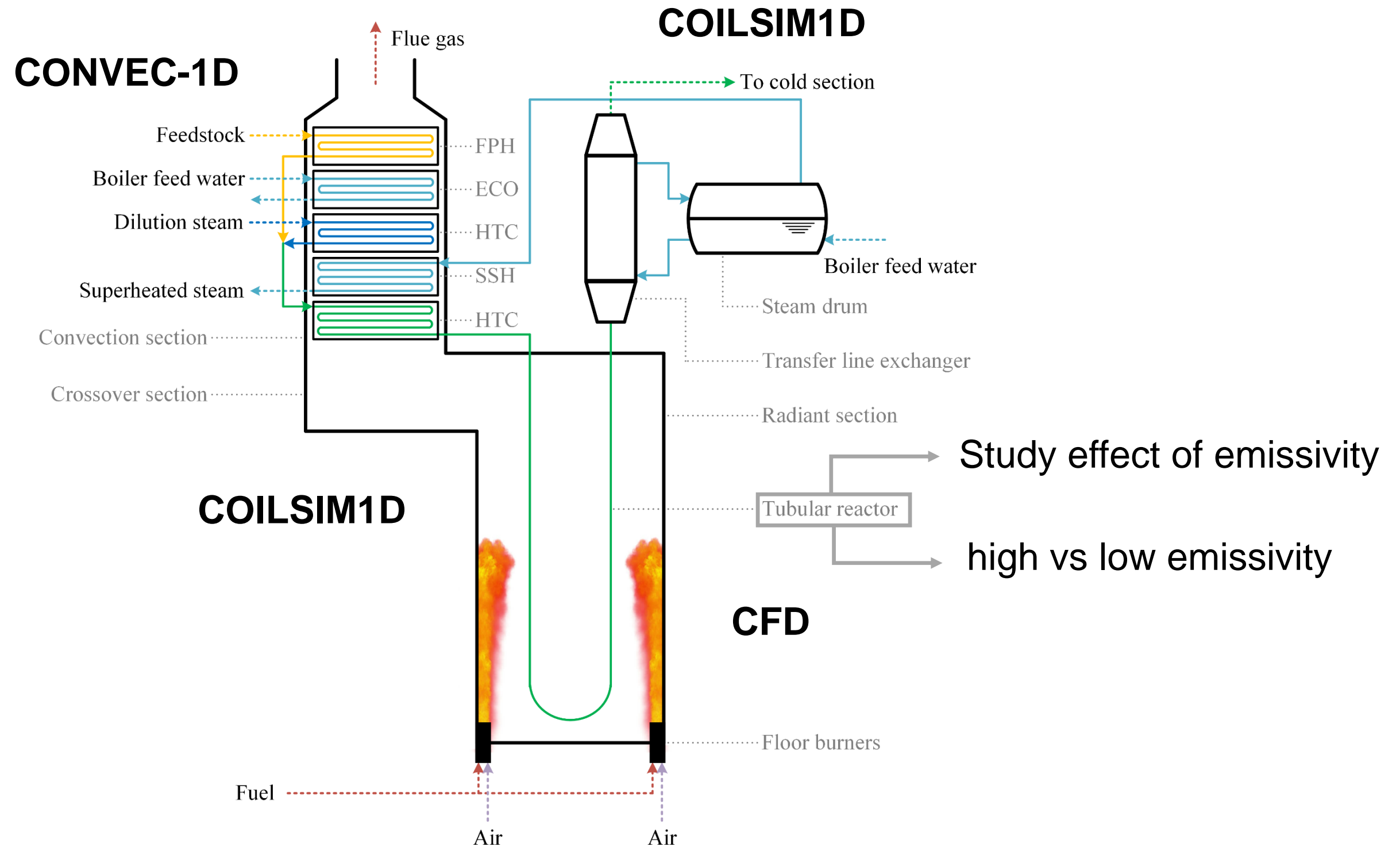
²Schmidt & Clemens

Introduction: the steam cracking process

Hydrocarbon feed is cracked at high temperatures to produce light olefins



Commodity
chemicals



Introduction: emissivity

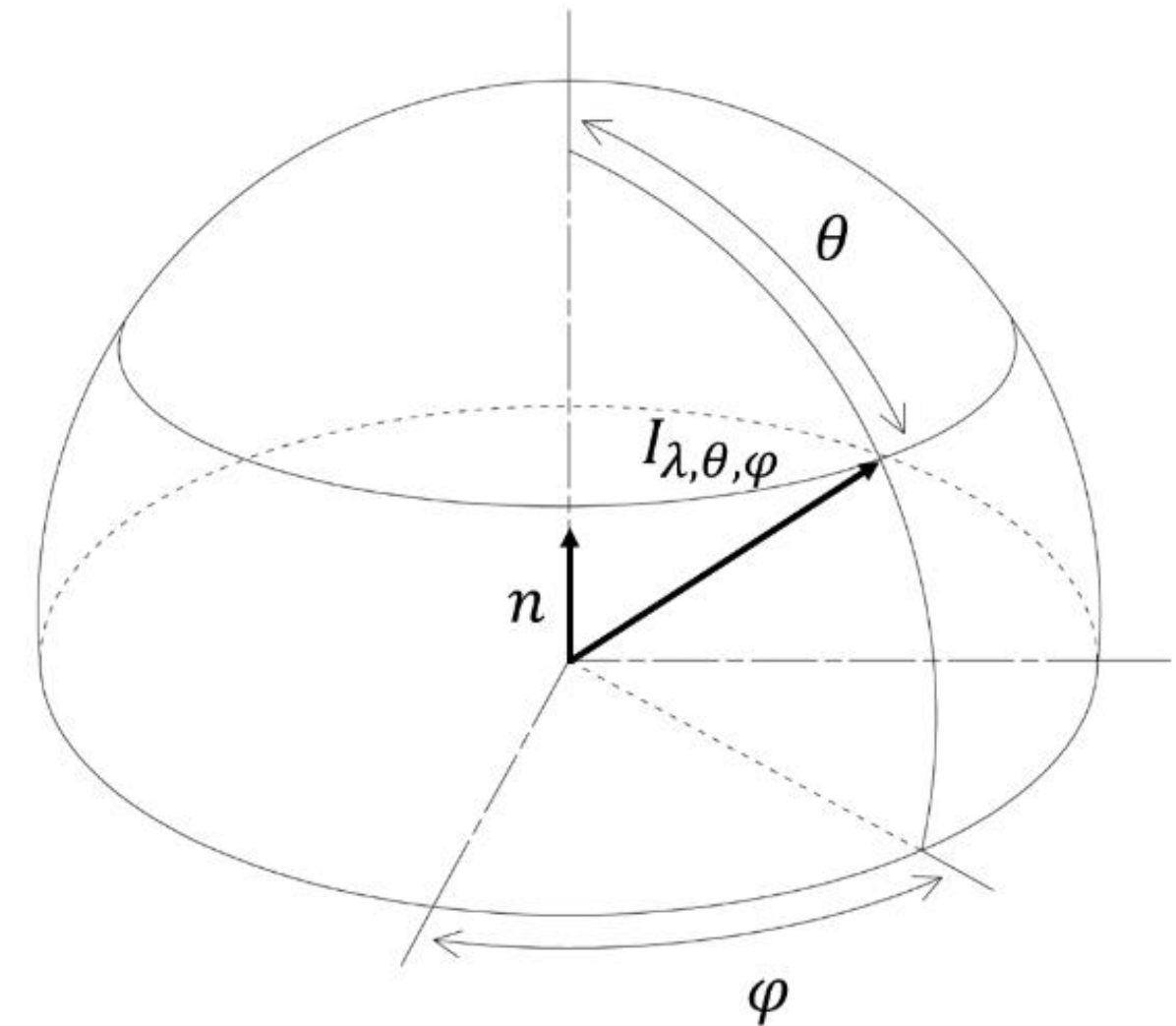
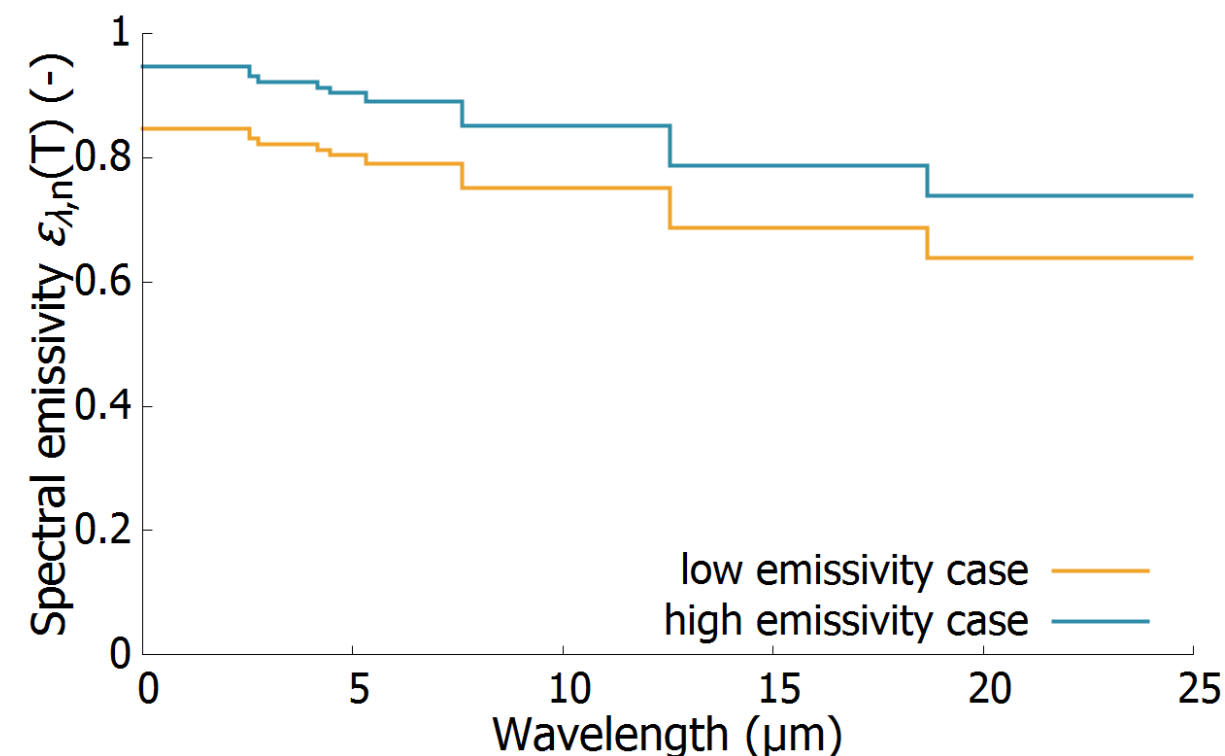
The **emissivity** is a measure for the deviation of the surface irradiance from a perfect blackbody.

The most fundamental emissive property is the **spectral directional emissivity**:

$$\varepsilon_{\lambda,\theta,\varphi}(\lambda, \theta, \varphi, T) = \frac{I_{\lambda,\theta,\varphi}(\lambda, \theta, \varphi, T)}{I_{\lambda}^B(\lambda, T)}$$



accounting for
spectral dependency



Introduction: radiative heat transfer

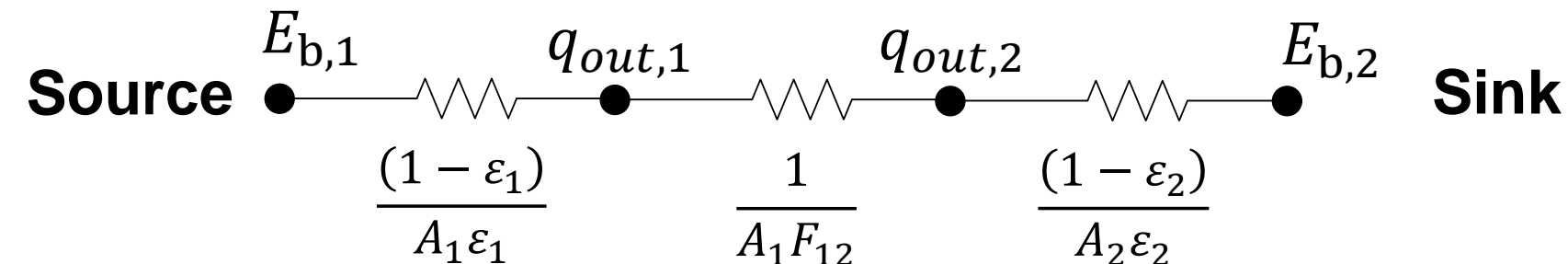
Radiative energy balance on a process tube

$$\begin{aligned} q_{inci} &= q_{net} + q_{out} \\ &= q_{net} + q_{refl} + q_{emit} \\ &= q_{net} + (1 - \varepsilon)q_{inci} + \varepsilon\sigma T^4 \end{aligned}$$

Total heat supplied to process gas

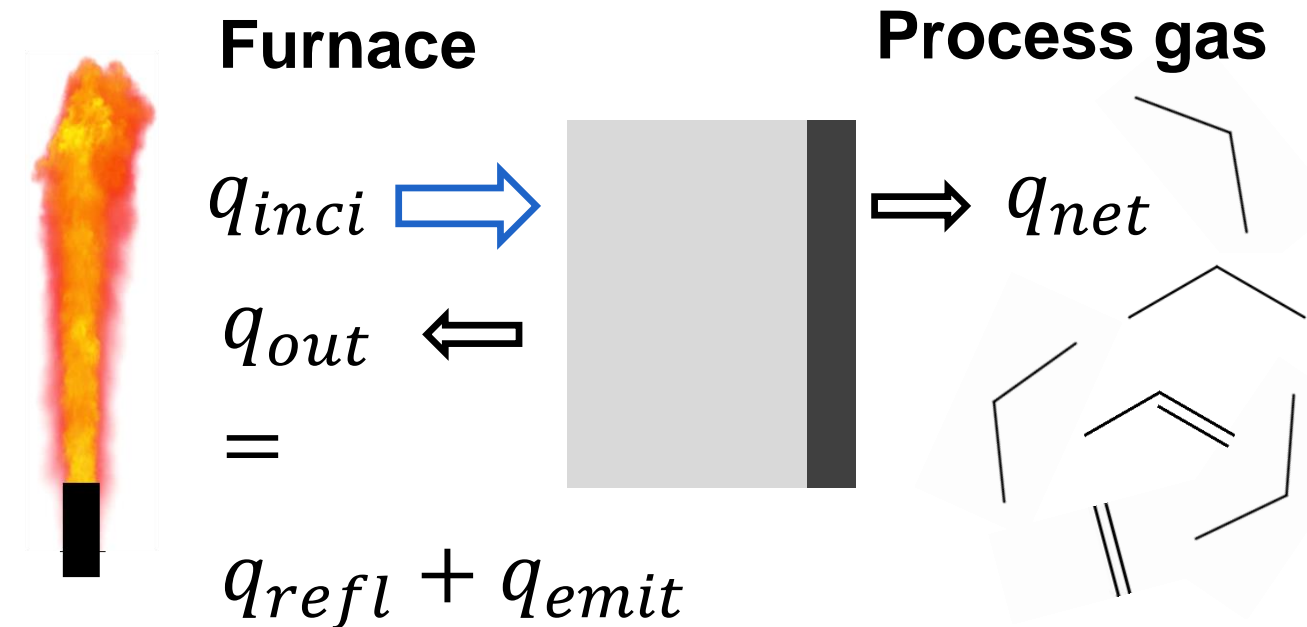
$$Q = A \cdot q_{net} = A[q_{inci} - q_{out}] = A \left[\frac{q_{out} - \varepsilon E_b}{1 - \varepsilon} - q_{out} \right] = \frac{q_{out} - E_b}{\left(\frac{1 - \varepsilon}{A \varepsilon} \right)}$$

This way the “**electric circuit analogy**” can be introduced:



Total heat transfer from source to sink:

$$Q_{1,2} = \frac{E_{b,1} - E_{b,2}}{\frac{(1 - \varepsilon_1)}{A_1 \varepsilon_1} + \frac{1}{A_1 F_{12}} + \frac{(1 - \varepsilon_2)}{A_2 \varepsilon_2}}$$

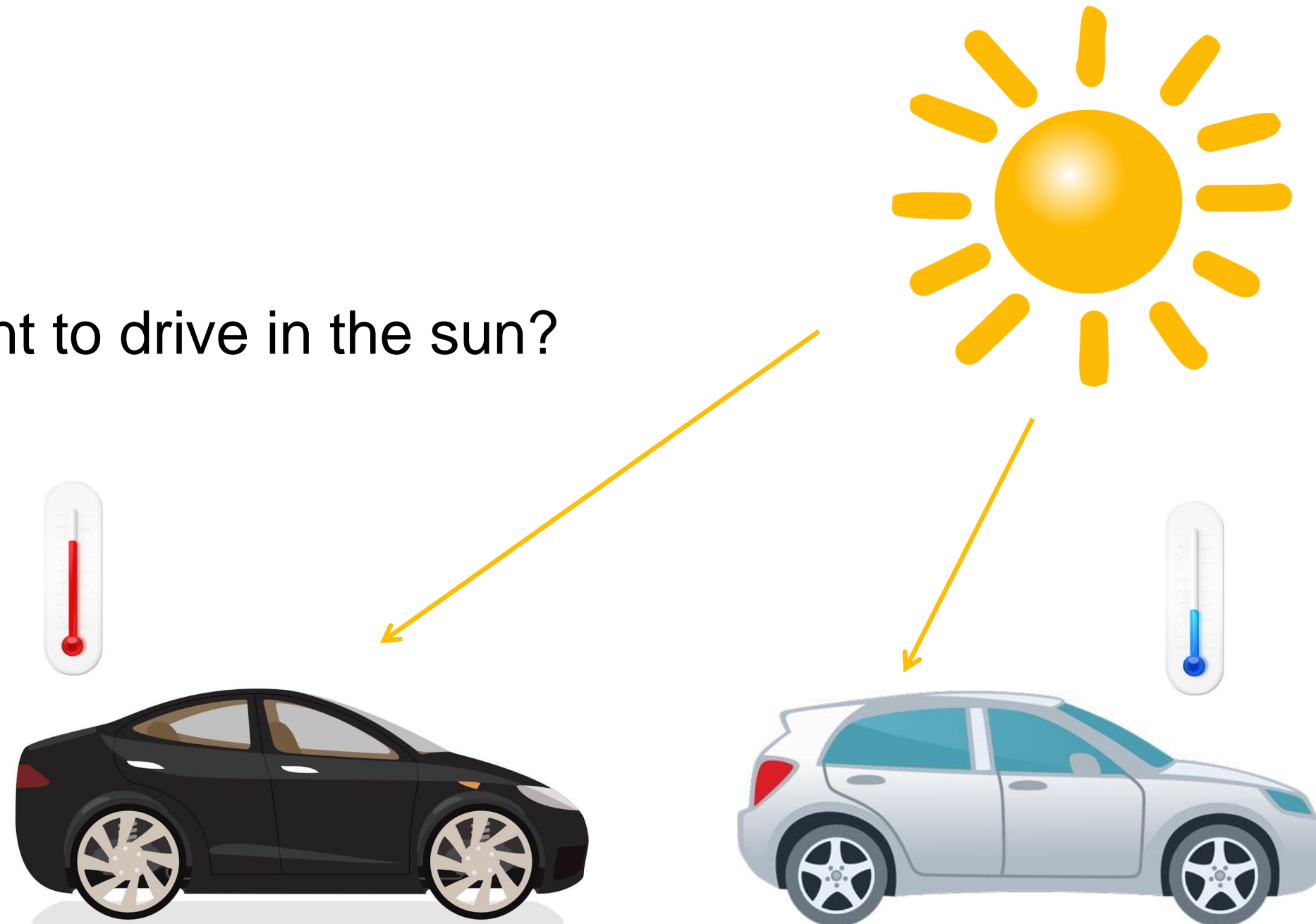


Introduction: absorption

Radiative heat transfer between two surfaces: example

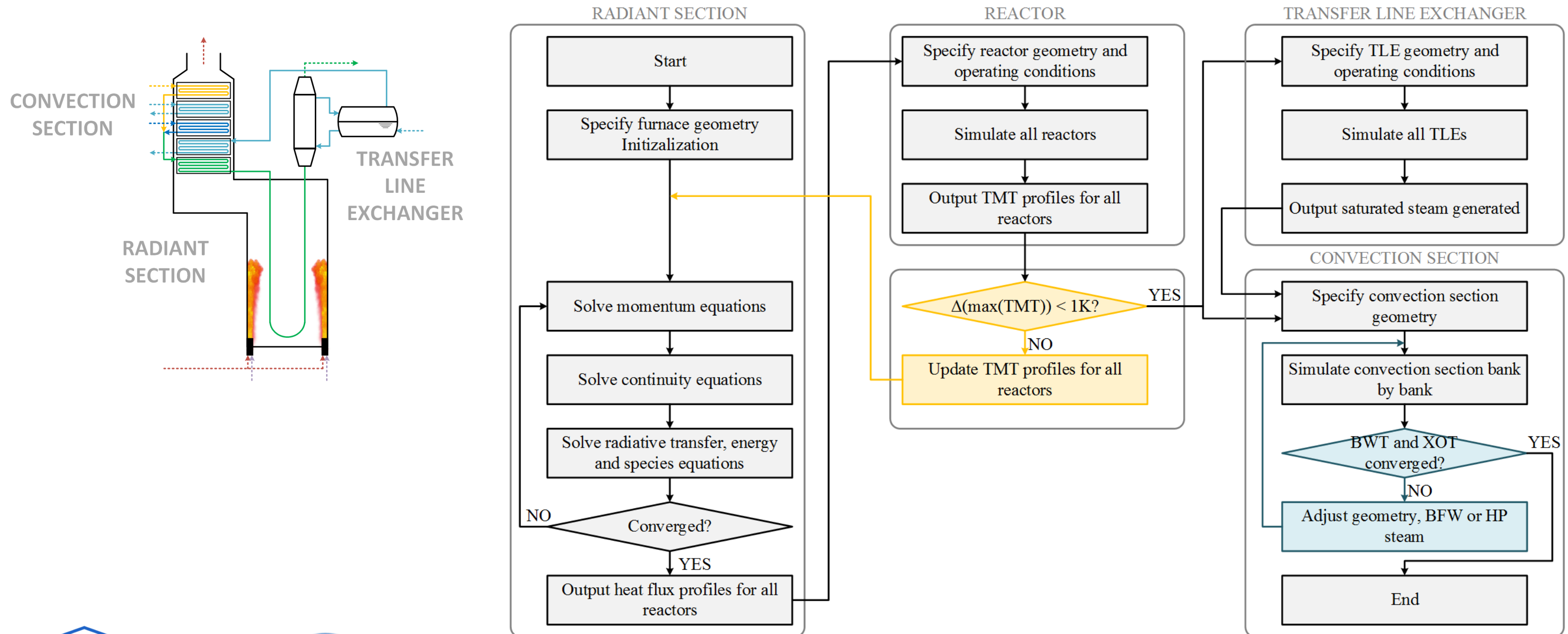
$$Q_{1,2} = \frac{E_{b,1} - E_{b,2}}{\frac{1}{A_1 F_{12}} + \frac{(1 - \varepsilon_2)}{A_2 \varepsilon_2}}$$

Which car would you want to drive in the sun?



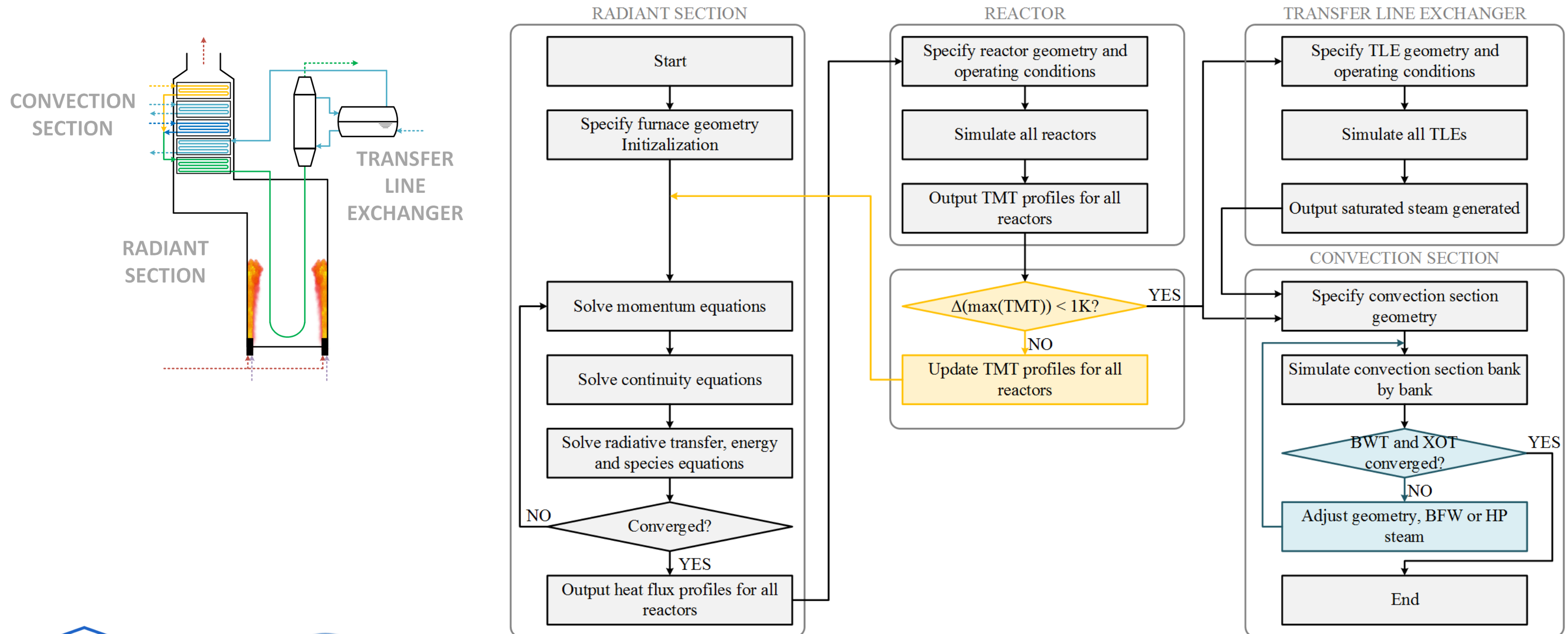
Simulation procedure: low emissivity case

Compare high vs low emissivity coil coating



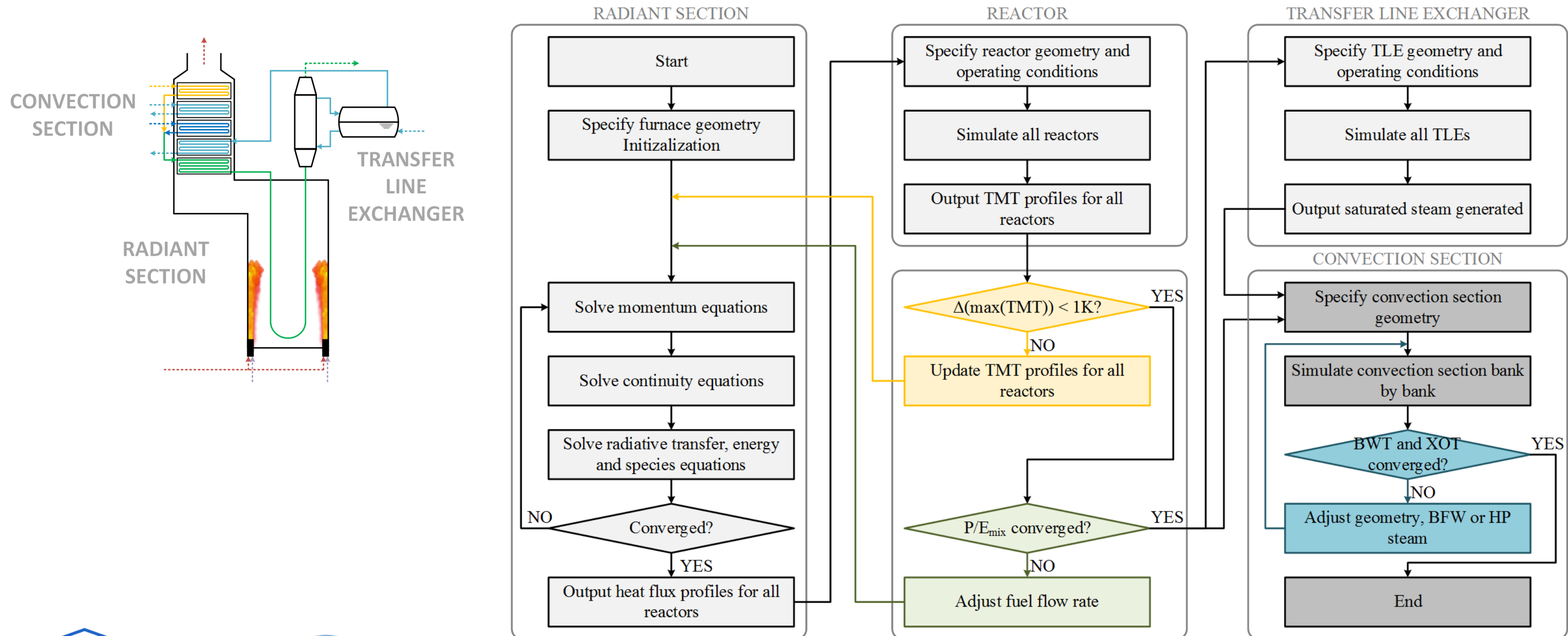
Simulation procedure: high emissivity case

Higher coil emissivity \rightarrow more energy to process gas \rightarrow over cracking



Simulation procedure: high emissivity case

Higher coil emissivity \rightarrow more energy to process gas \rightarrow over cracking \rightarrow reduce fuel

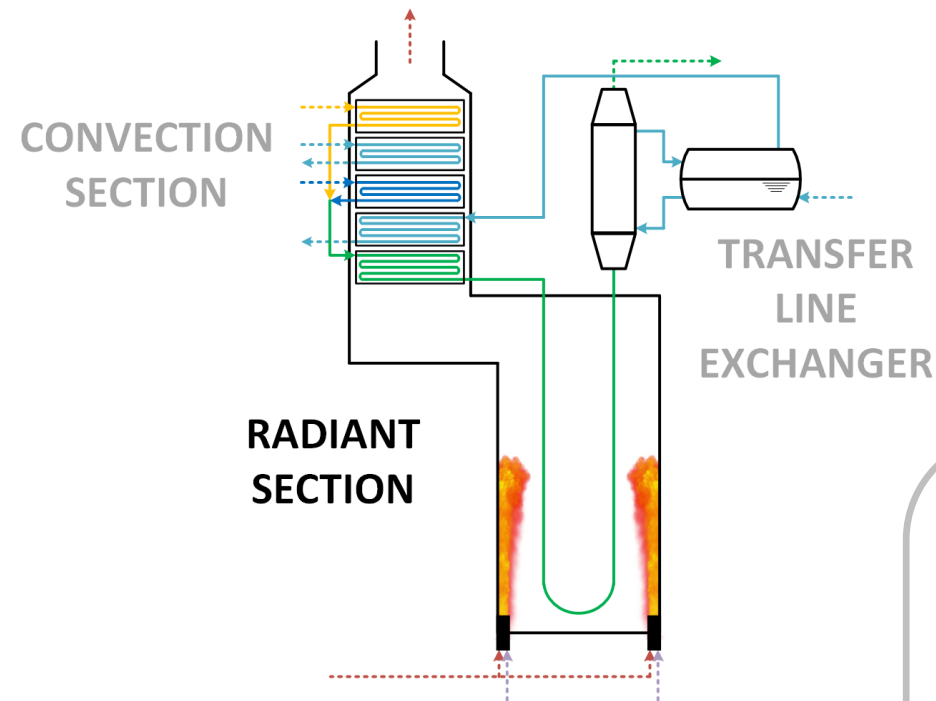


Geometry & operating conditions

Ultra Selective Conversion (USC) furnace simulated by [Zhang et al.](#):

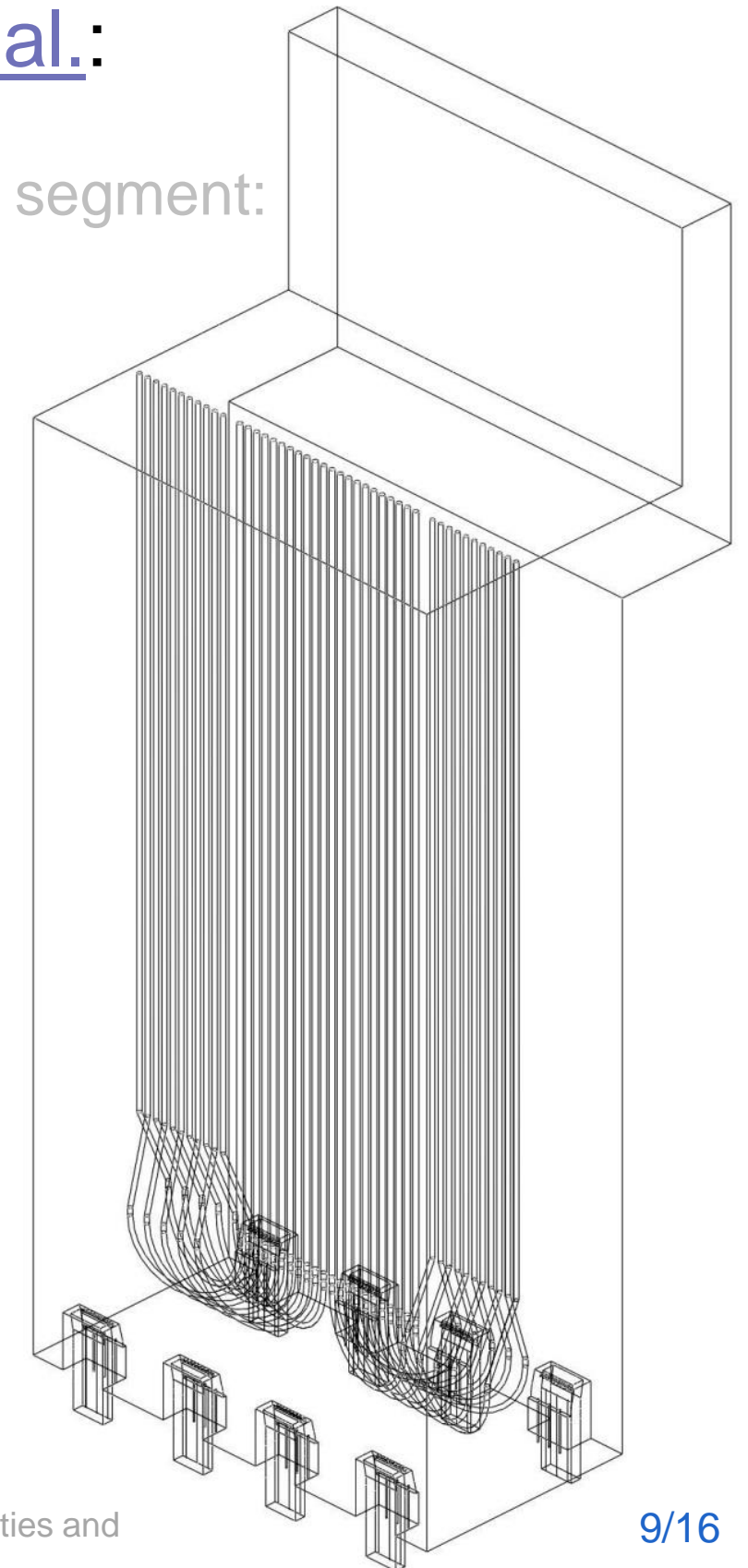
- 100 % floor fired
- U-coil reactor
- 22 reactor coils
- Naphtha feedstock

Simulated furnace segment:



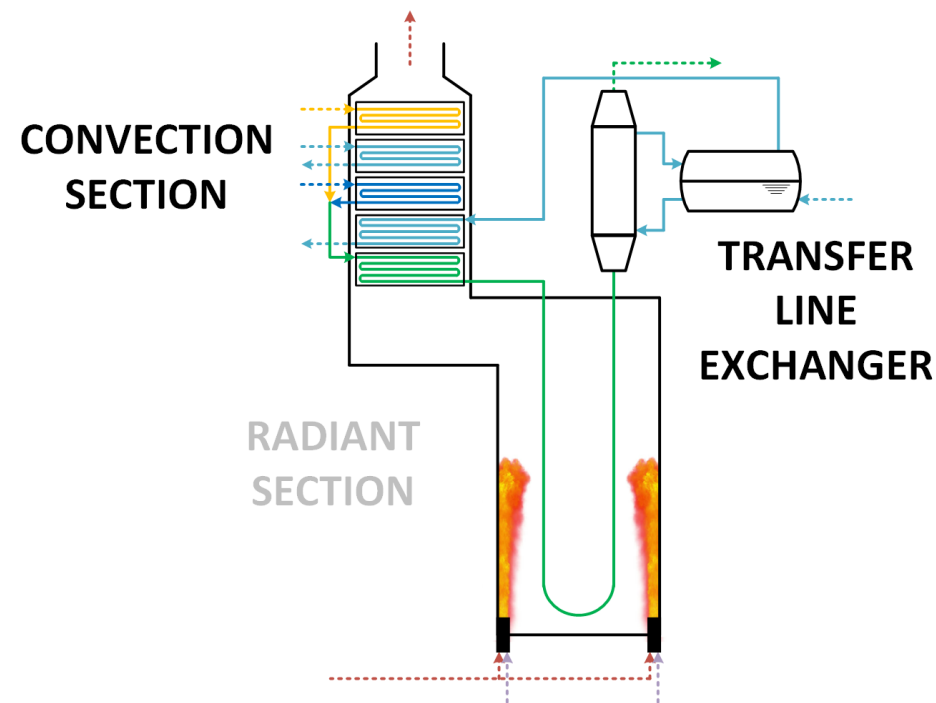
Numerical models – CFD and COILSIM1D

- RANS $k-\varepsilon$ turbulence modelling
- Discrete ordinates radiation using an exponential wide band model
- Two-step combustion model
- TMT coupling with COILSIM1D



Geometry & operating conditions

Convection section as simulated by [Verhees et al.](#):



Numerical models – CONVEC-1D

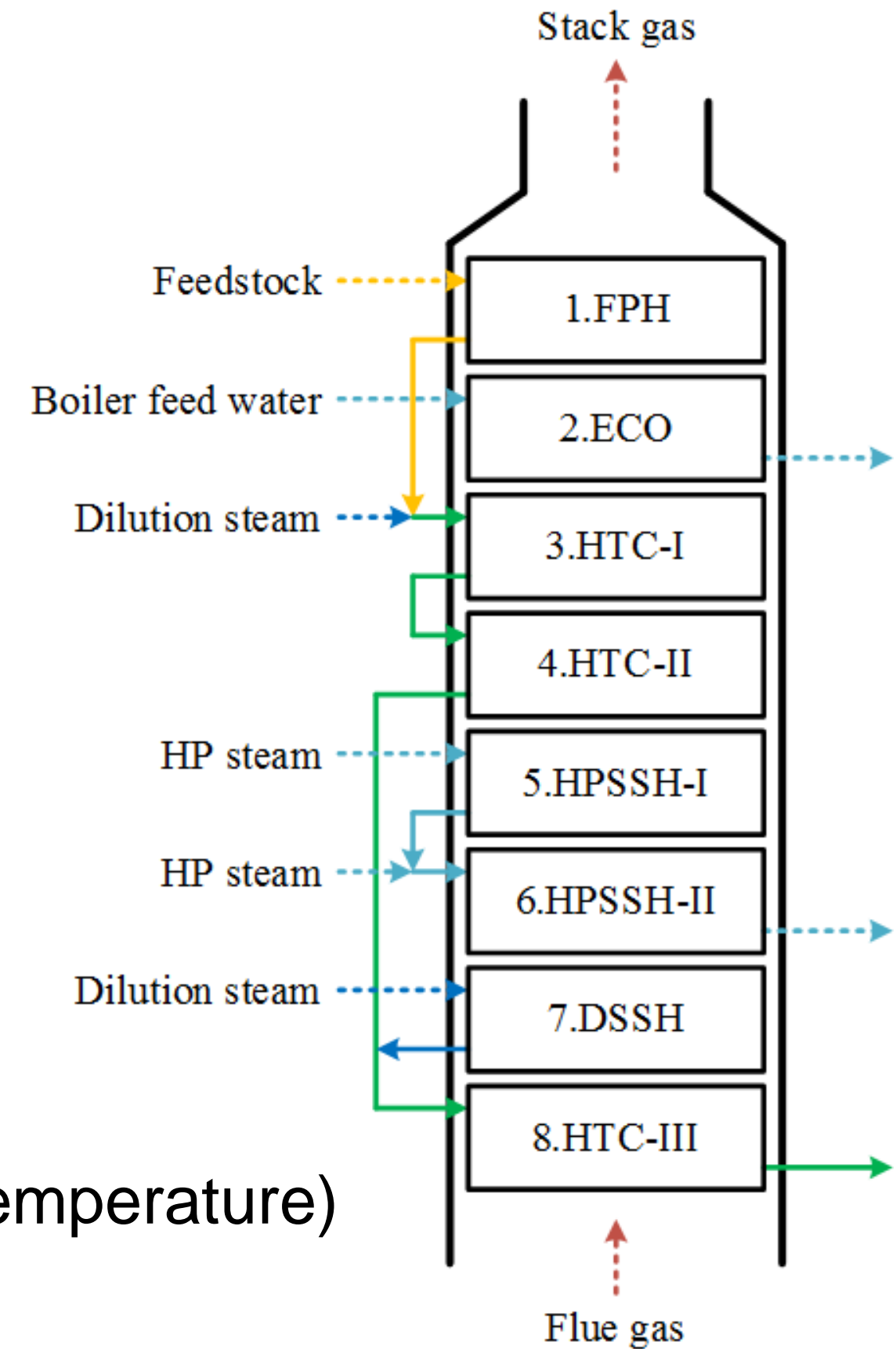
1D heat transfer simulation tool

Process gas side:

- Two phase boiling models

Flue gas side:

- Convective flow over horizontal bank



Transfer line exchanger: ultraselective quench cooler

Double pipe exchanger combining two coils (770 K outlet temperature)

Simulation results: low emissivity case

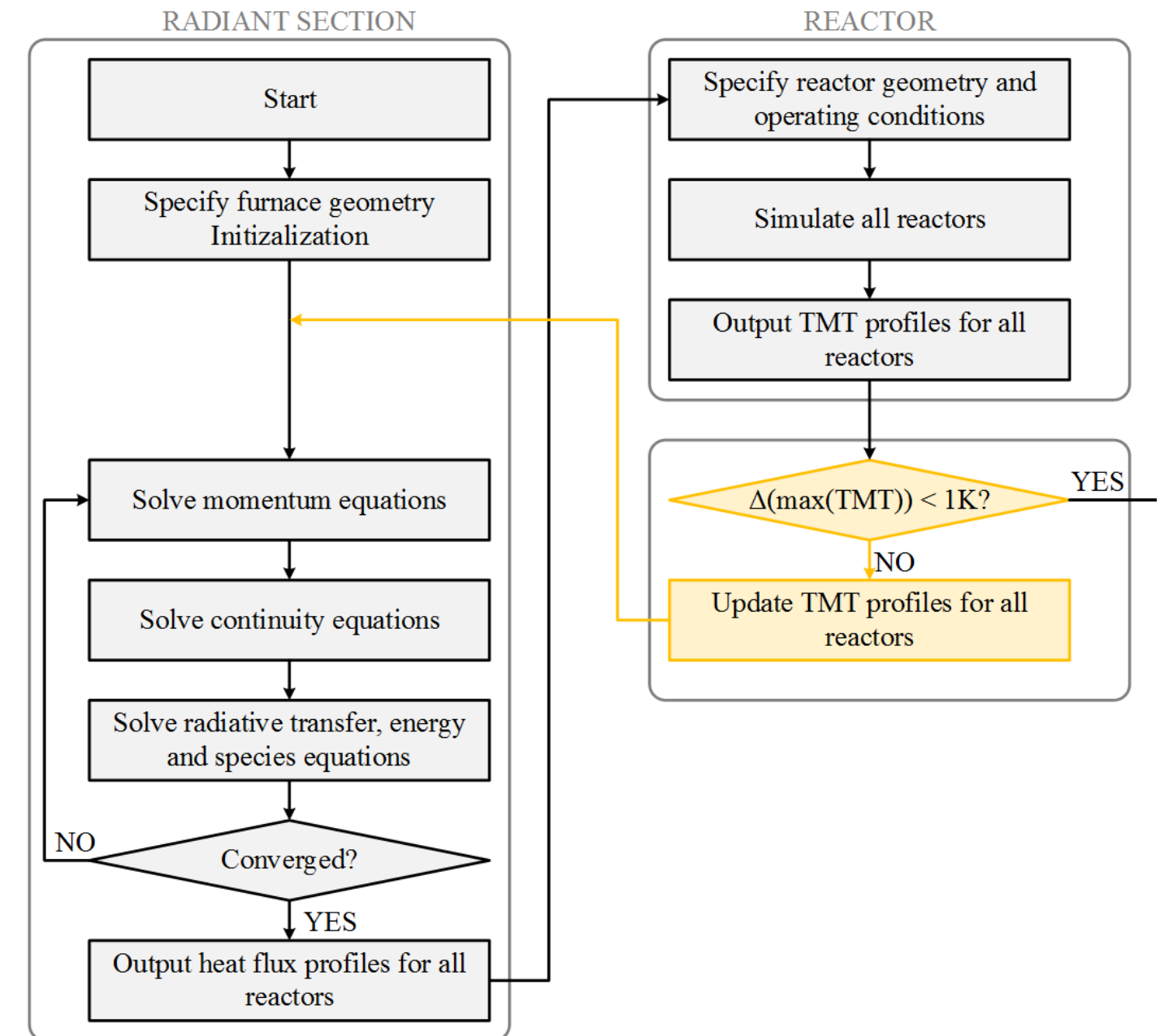
Simulation results radiant section

Radiant section

Total fuel flow rate [kg/s]	1.1108
Flue gas bridge wall temperature [K]	1370
Percent of total heat flux via radiation [%]	77.88

Reactor

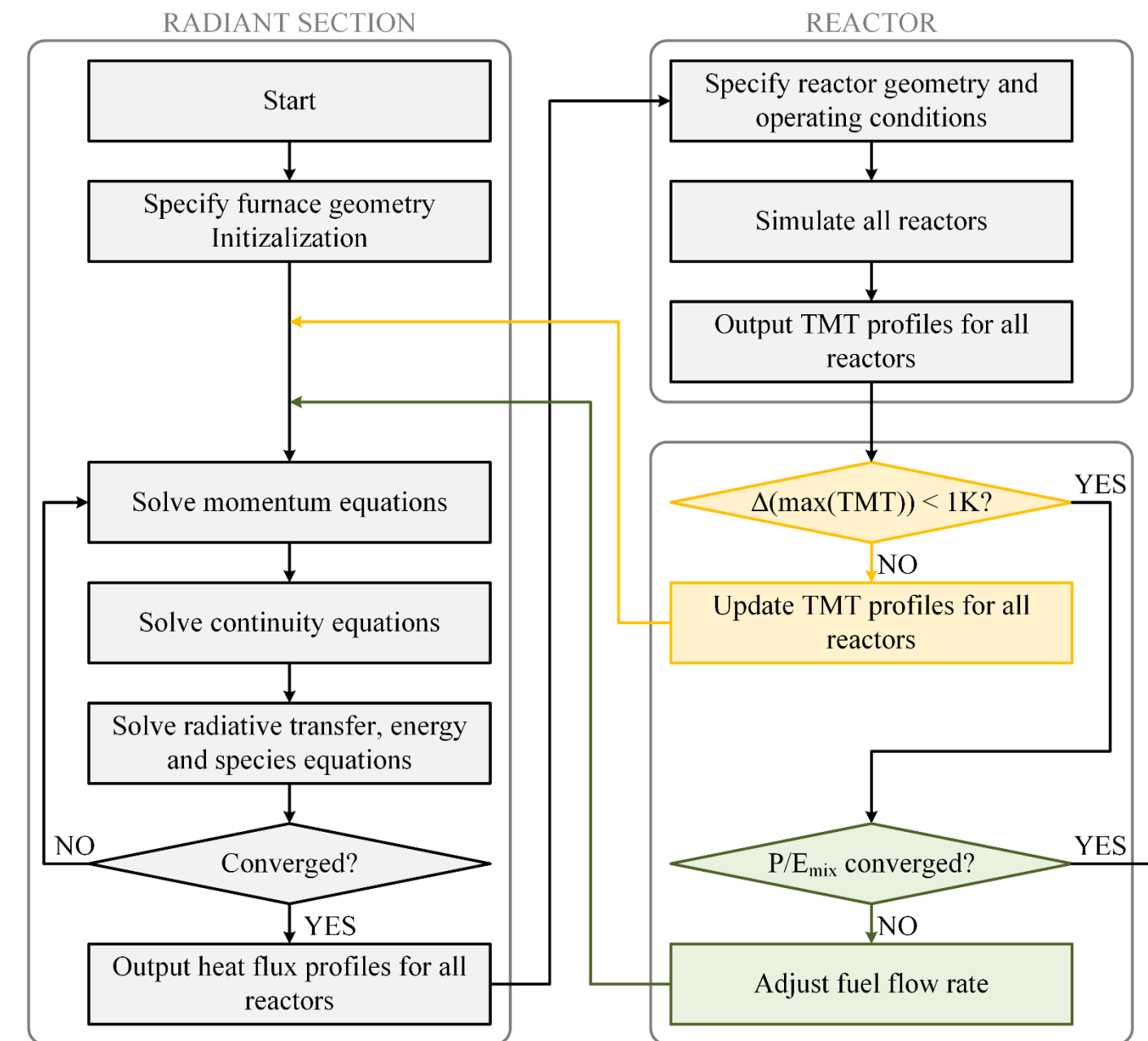
Mixing-cup average COT [K]	1146.1
Average ethene yield [wt%]	28.89
Average propene yield [wt%]	15.25
Mixing-cup average P/E	0.5284



Simulation results: low vs high emissivity case

Simulation results radiant section

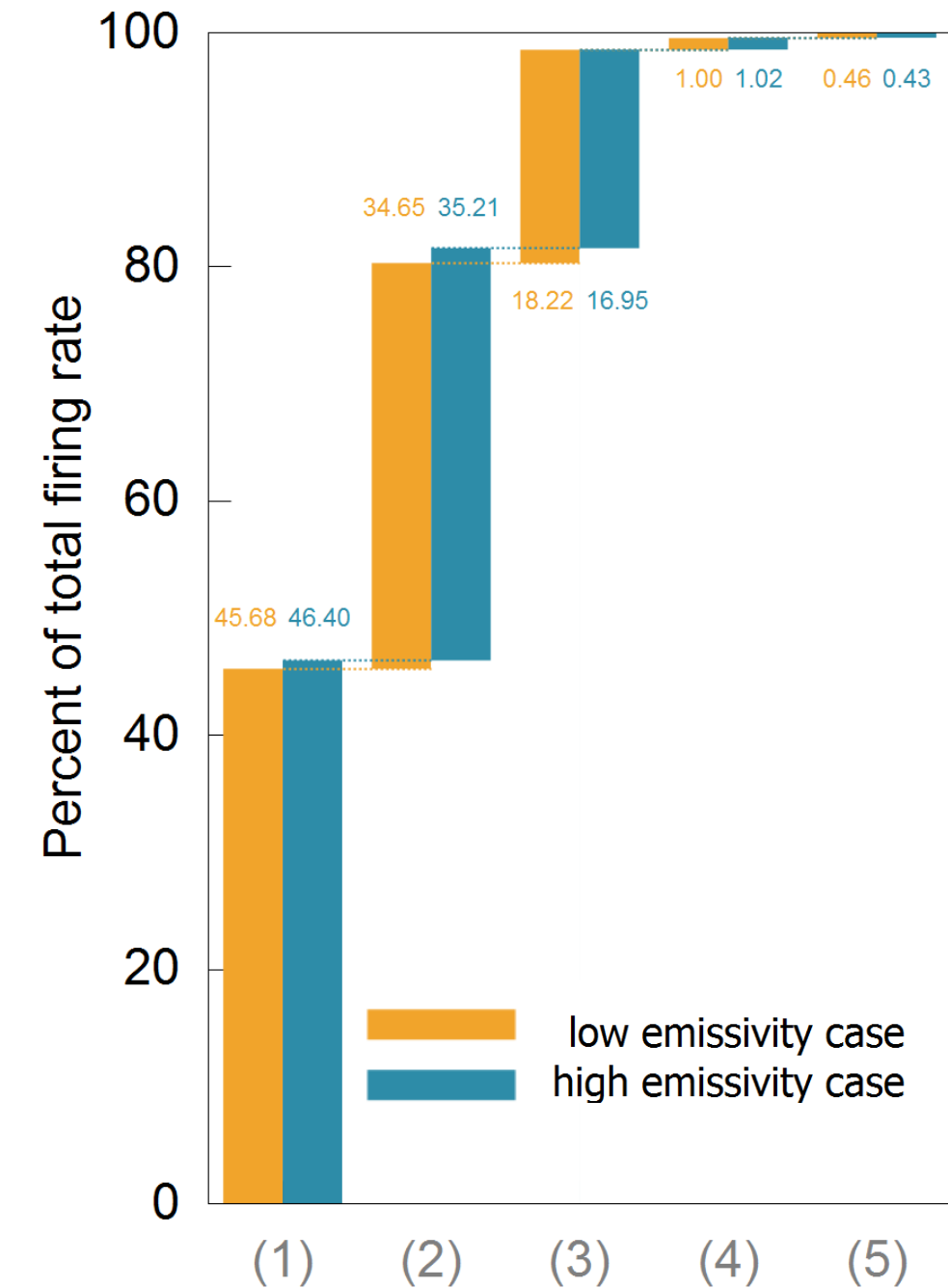
	low emissivity	high emissivity
Radiant section		
Total fuel flow rate [kg/s]	1.1108	1.0916 ↓
Flue gas bridge wall temperature [K]	1370	1356 ↓
Percent of total heat flux via radiation [%]	77.88	79.33 ↑
Reactor		
Mixing-cup average COT [K]	1146.1	1145.3
Average ethene yield [wt%]	28.89	28.88
Average propene yield [wt%]	15.25	15.25
Mixing-cup average P/E	0.5284	0.5284



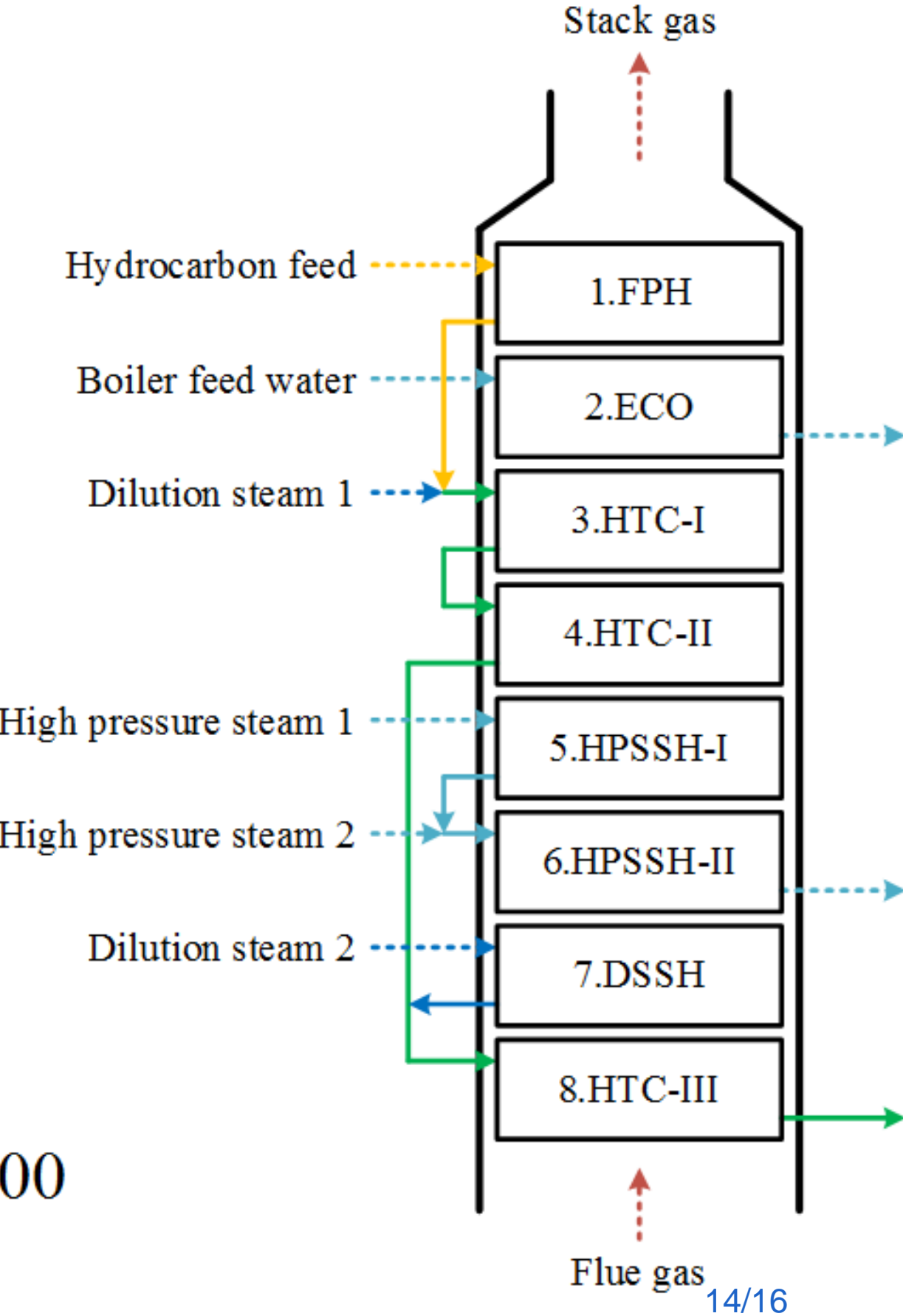
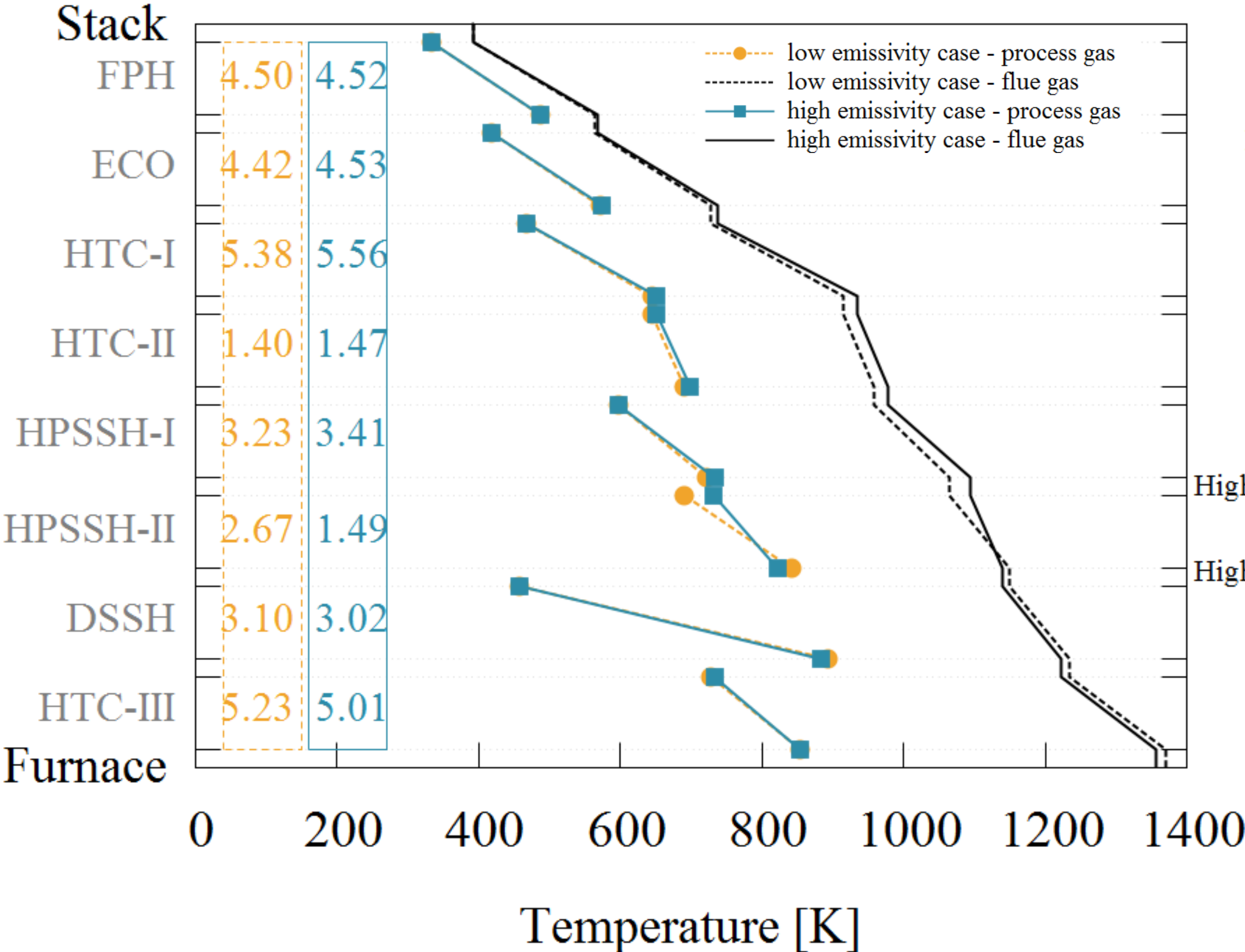
Overall energy balance

After performing convection section and transfer line exchanger simulations

	low emissivity	high emissivity	
Total fired duty [kW]	56628	55652	↓
(1) Total reactor duty [kW]	25868	25820	~
(2) Total preheating duty convection section [kW]	19620	19593	~
(3) Total energy recovery duty convection section [kW]	10316	9435	↓
(4) Total losses from radiant section [kW]	566	566	~
(5) Total losses through stack [kW]	259	238	↓
Furnace efficiency radiant section [%]	45.68	46.40	↑



Closer look at the energy balance

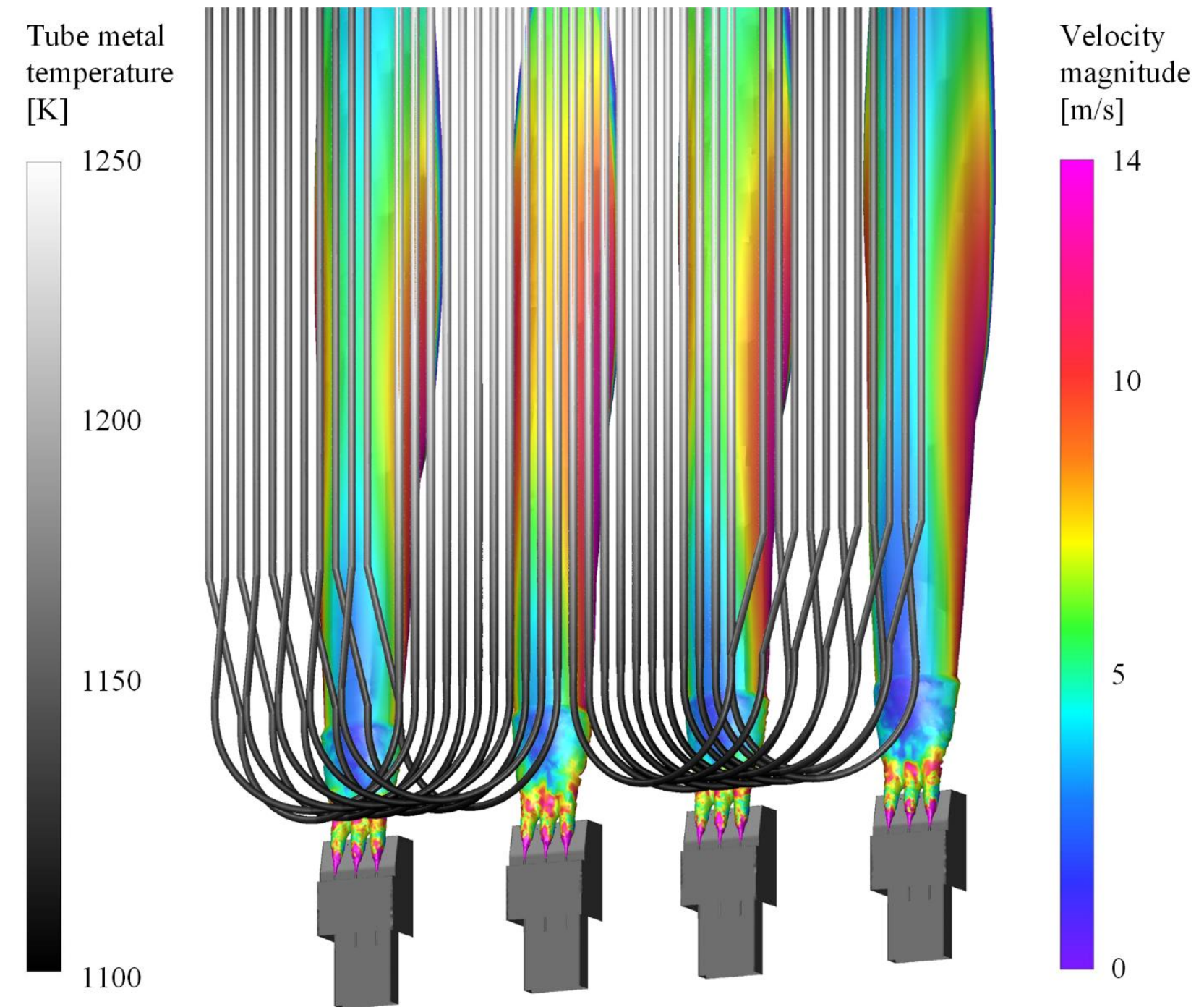


Conclusions

Increasing the coil emissivity results in:

- Increased energy efficiency of the radiant section by 0.70 % absolute
- Reduced firing rate by 1.73 %
- Reduced bridge wall temperature of 14 K

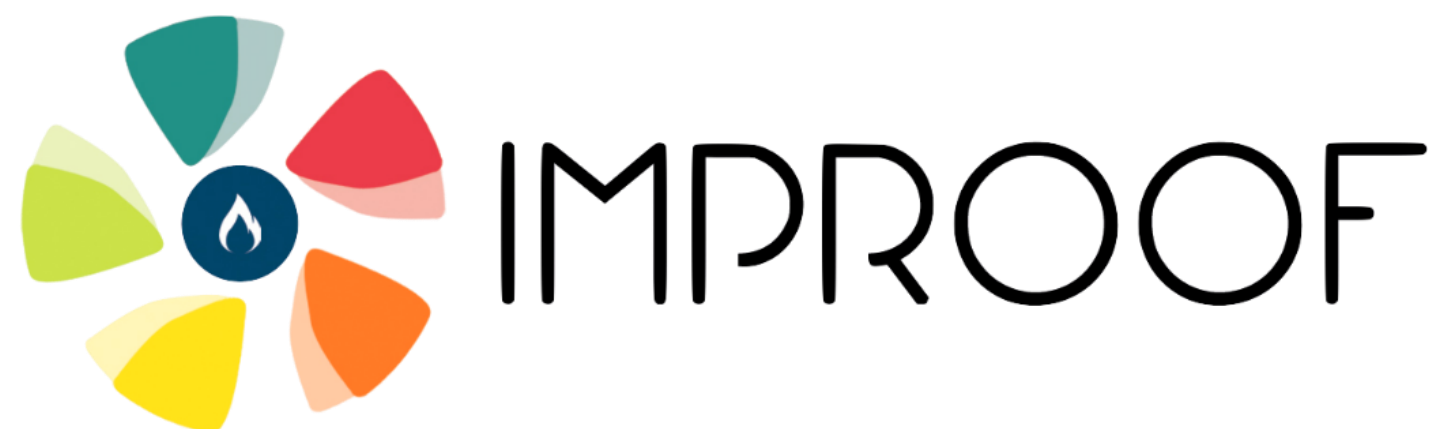
→ minor operating changes to convection section required



Acknowledgements

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